

# ECEN474: (Analog) VLSI Circuit Design

## Fall 2011

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### Lecture 20: Common-Mode Feedback Circuits



Sebastian Hoyos  
Analog & Mixed-Signal Center  
Texas A&M University

# Agenda

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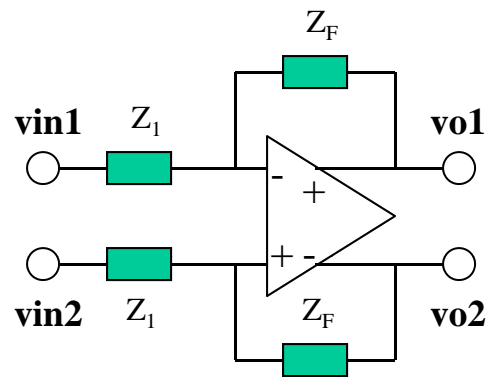
- Common-Mode Feedback Circuits

A photograph of a multi-pin connector, possibly a ribbon cable connector, with a white label overlaid on it. The label contains text about common-mode feedback circuits. The background shows the metal pins and the green printed circuit board (PCB) of the connector.

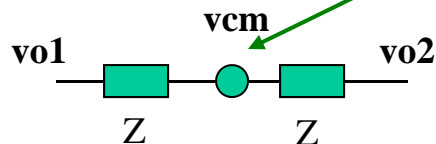
## What is a common-mode feed-back correction circuit ?

A common mode **feed-back** circuit is a circuit sensing the common-mode voltage, comparing it with a proper reference, and feeding back the correcting common-mode signal (both nodes of the fully-differential circuit) with the purpose to cancel the output common-mode current component, and to fix the dc outputs to the desired level.

## Fully-Differential Filters: CMFB Principle



Simplest common-mode detector



$$v_{cm} = \frac{v_{o1} + v_{o2}}{2}$$

➤ A common-mode feedback loop must be used: Circuit must operate on the common-mode signals only!

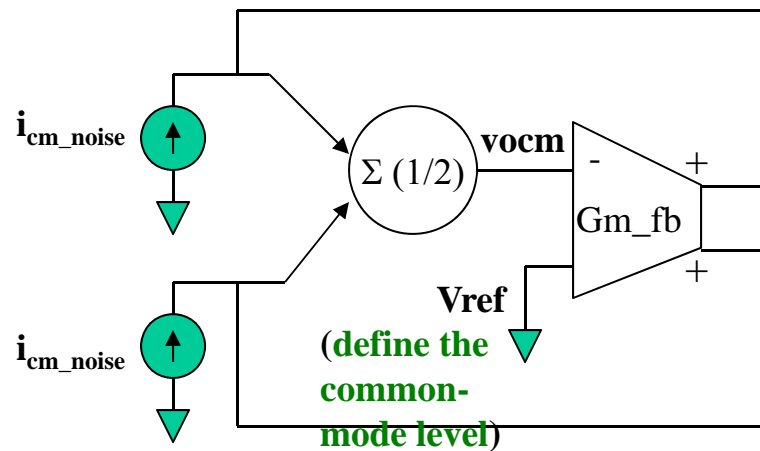
➤ BASIC IDEA: CMFB is a circuit with very small impedance for the common-mode signals but transparent for the differential signals.

➤ Use a common-mode detector (eliminates the effect of differential signals and detect common-mode signals)

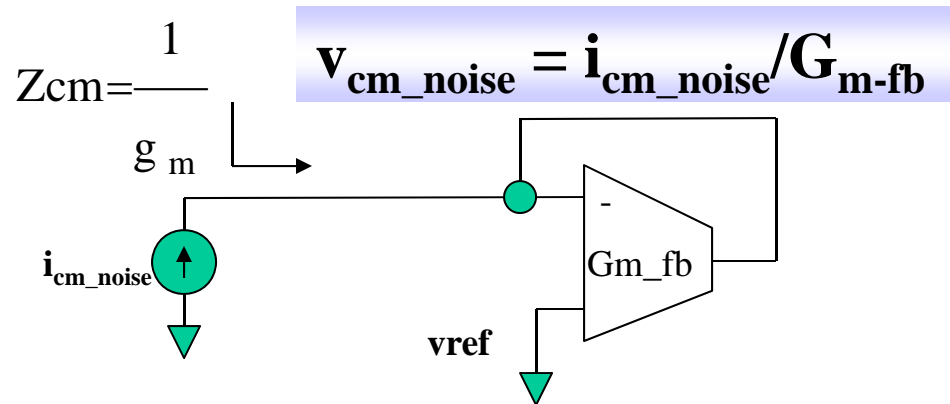
➤ Analyze the common-mode feedback loop: Large transconductance gain and enough phase margin

➤ Minimum power consumption

## CMFB Principles: Analysis of the loop for common-mode signals only



### ↓ Effect of common-mode noise:



➤ Analysis for common-mode noise; for instance noise due to power supplies:

➤  $i_{o1} = i_{o2} = i_{cm\_noise}$

➤ **The two outputs can be connected together for the analysis of the CMFB loop!**

#### ➤ BASIC CONCEPTS:

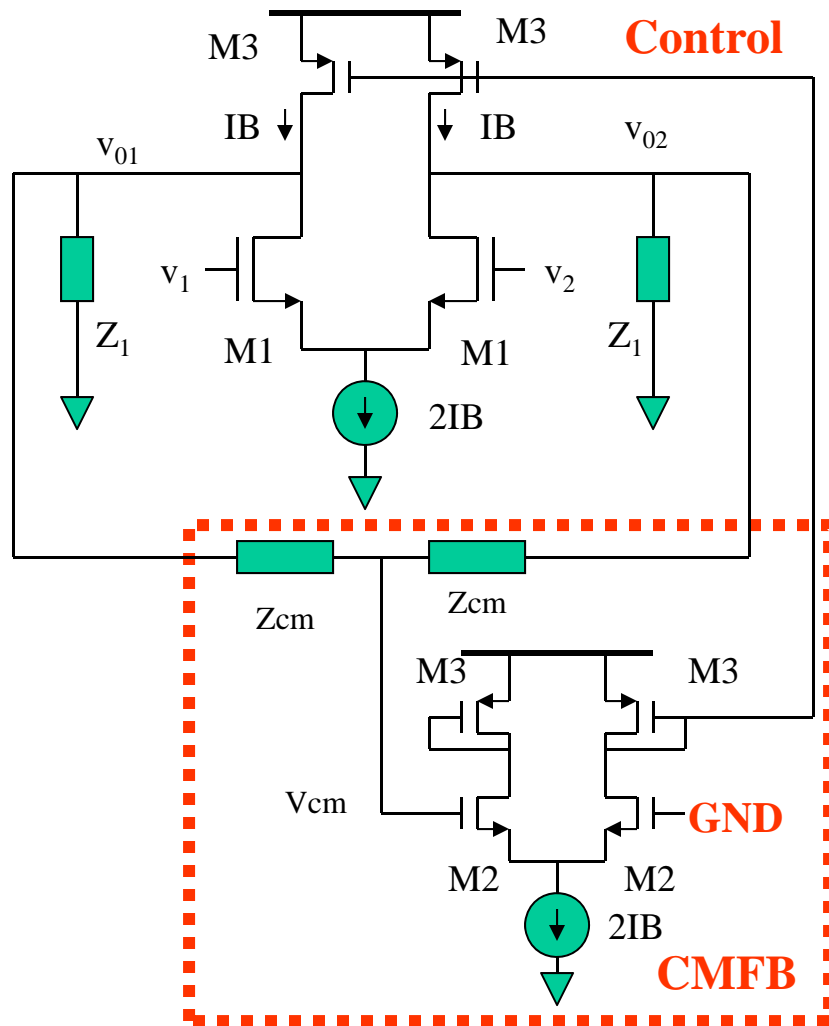
➤ The common-mode input noise is converted into a common-mode voltage (common-mode voltage noise) by the common-mode transconductance of the CMFB  $= 1/G_{m\_fb}$ .

➤ **common-mode voltage variations**

$$v_{cm\_noise} = i_{cm\_noise} / G_{m\_fb} !!$$

➤ **The larger  $G_{m\_fb}$  the smaller the effects of the common-mode noise!**

## Fully-Differential Filters: CMFB



### ➤ CMFB Characteristics:

➤ Transconductance gain =  $g_{m2}/2$  (no PMOS mirror in CMFB OTA)

➤ dominant pole at the output

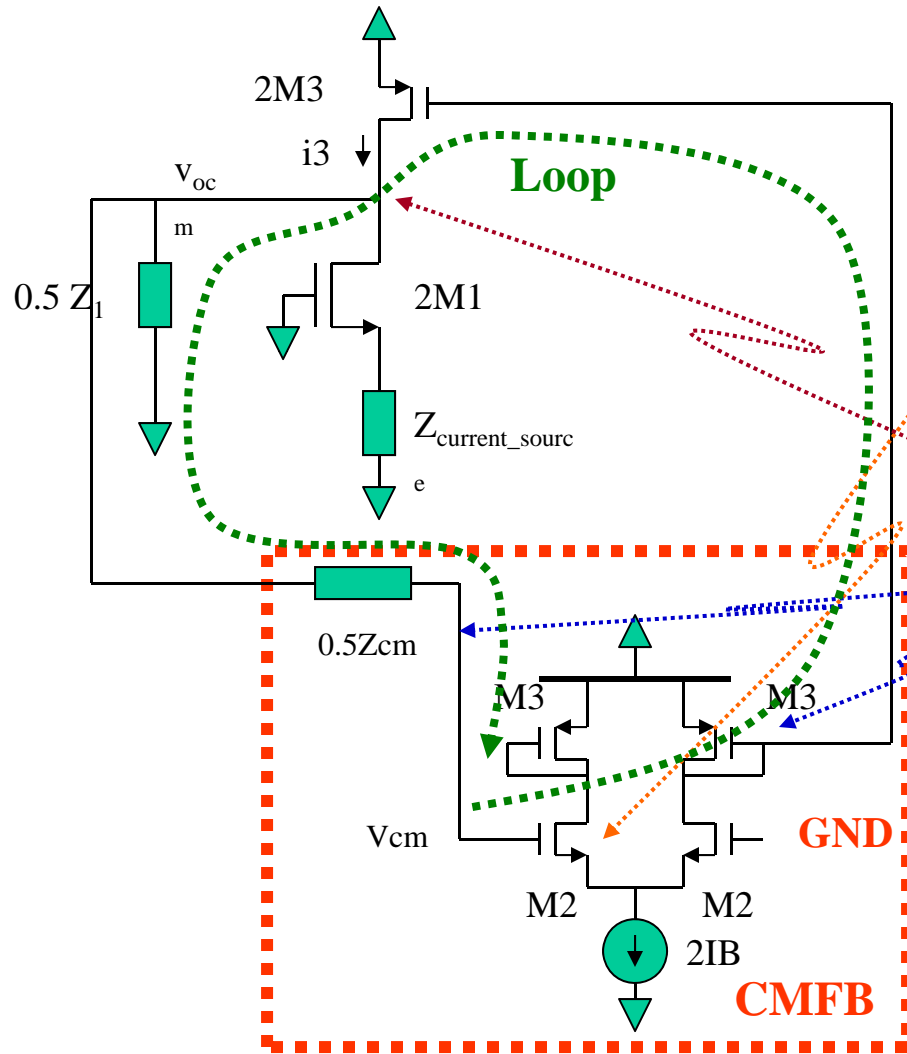
➤ At least 2 additional poles in the loop

➤  $Z_{cm}$  reduces the OTA dc gain, affecting the differential gain

➤ NOTE THAT  $V_{cm}$  IS FORCED TO BE AROUND THE GROUND LEVEL.

➤ DC OFFSET VOLTAGE IS AROUND  $2 \cdot I_{off}/g_{m2}$

## Fully-Differential Filters: CMFB



➤ **CMFB Characteristics:**

➤ DC Transconductance gain =  $g_{m2}/2$

➤ Loop gain (ignoring poles)

$$\approx \left( \frac{g_{m2}}{2} \right) \left( \frac{1}{g_{m3}} \right) (-2g_{m3}) \left( \frac{Z_1}{2} \right) = -\frac{g_{m2}Z_1}{2}$$

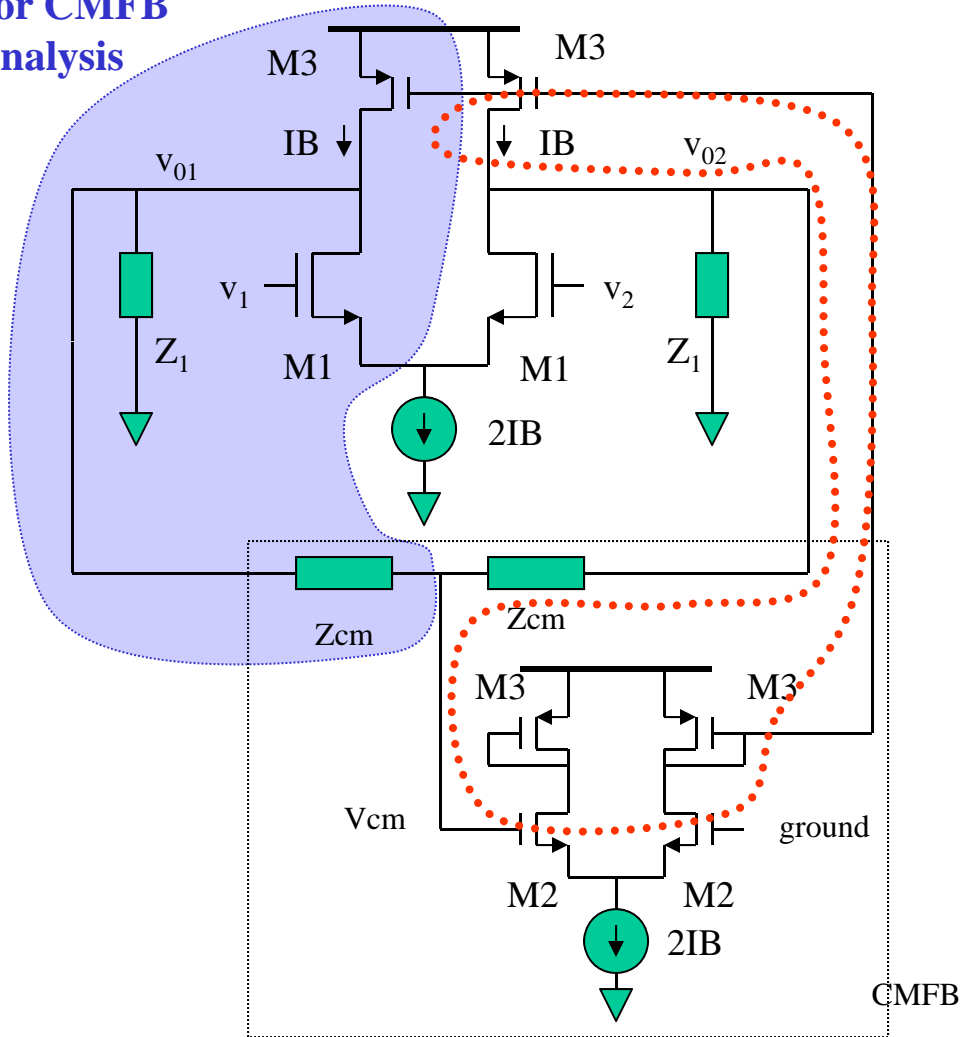
➤ dominant pole at the output

➤ At least 2 additional poles in the loop

➤ **DC OFFSET IS AROUND  $2I_{off}/g_{m2}$**

# Fully-Differential Filters: CMFB Principles

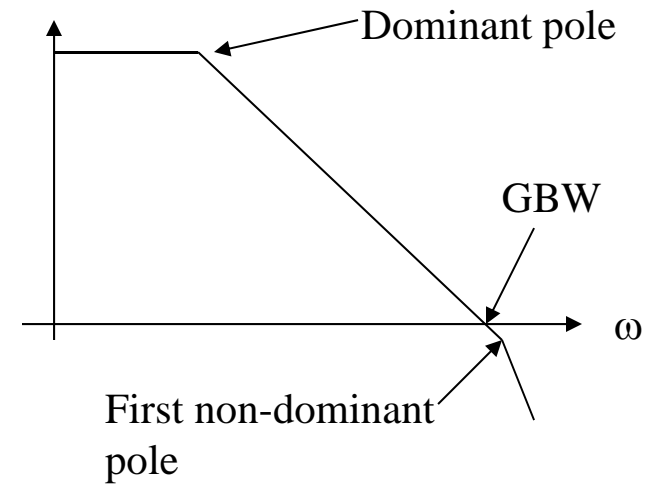
Can be removed for CMFB analysis



➤ Common-mode stability: DC gain and most relevant poles

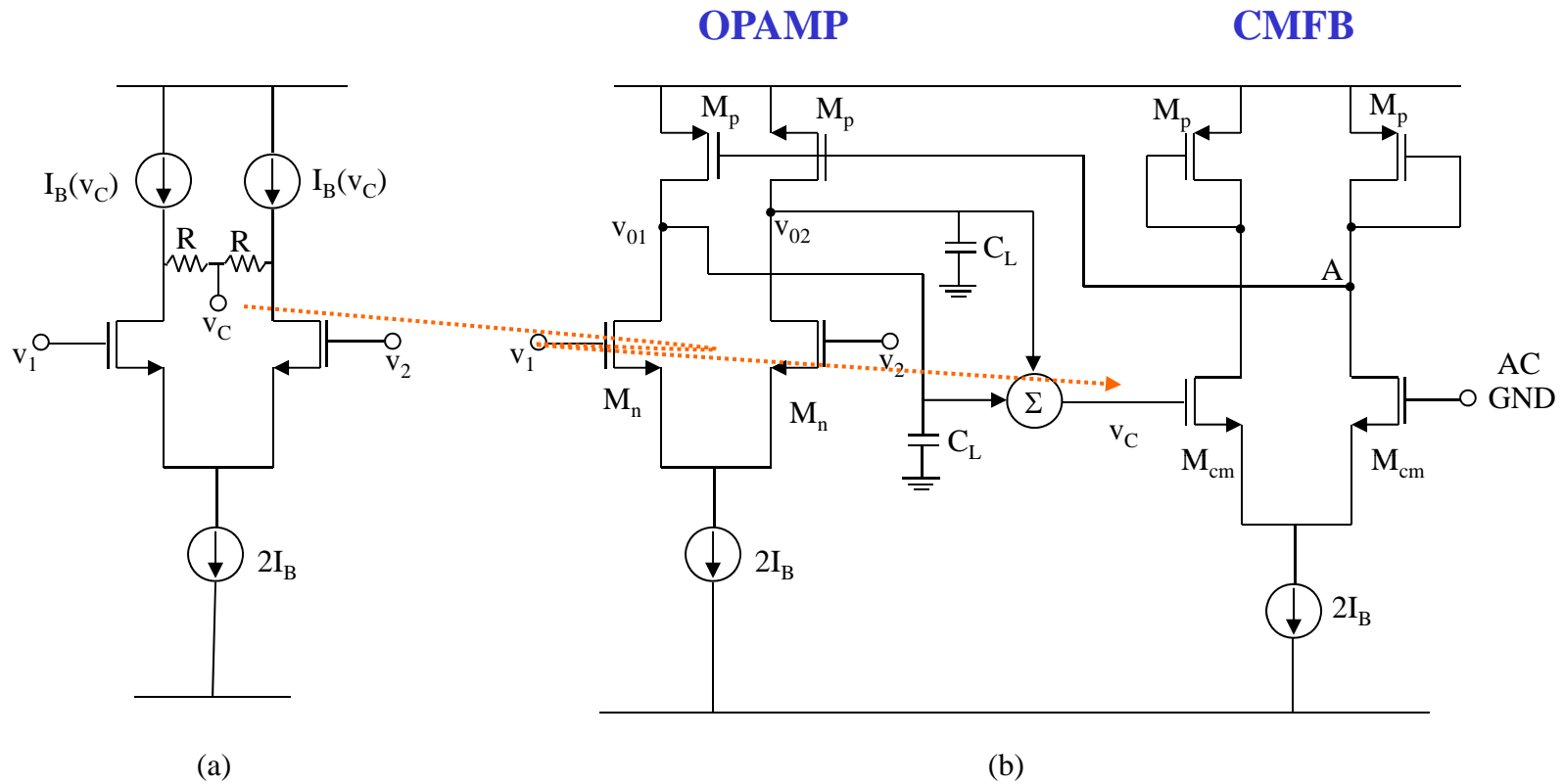
- 1 pole at vcm ( $1/RC$ )
- 1 pole at gate of M3 ( $g_{m3}/C_{P3}$ )
- 1 pole at the output ( $g_{o1}/C_1$ )

➤ dc gain =  $0.5 g_{m2}R_{o1}$



**Be sure phase margin > 45°**

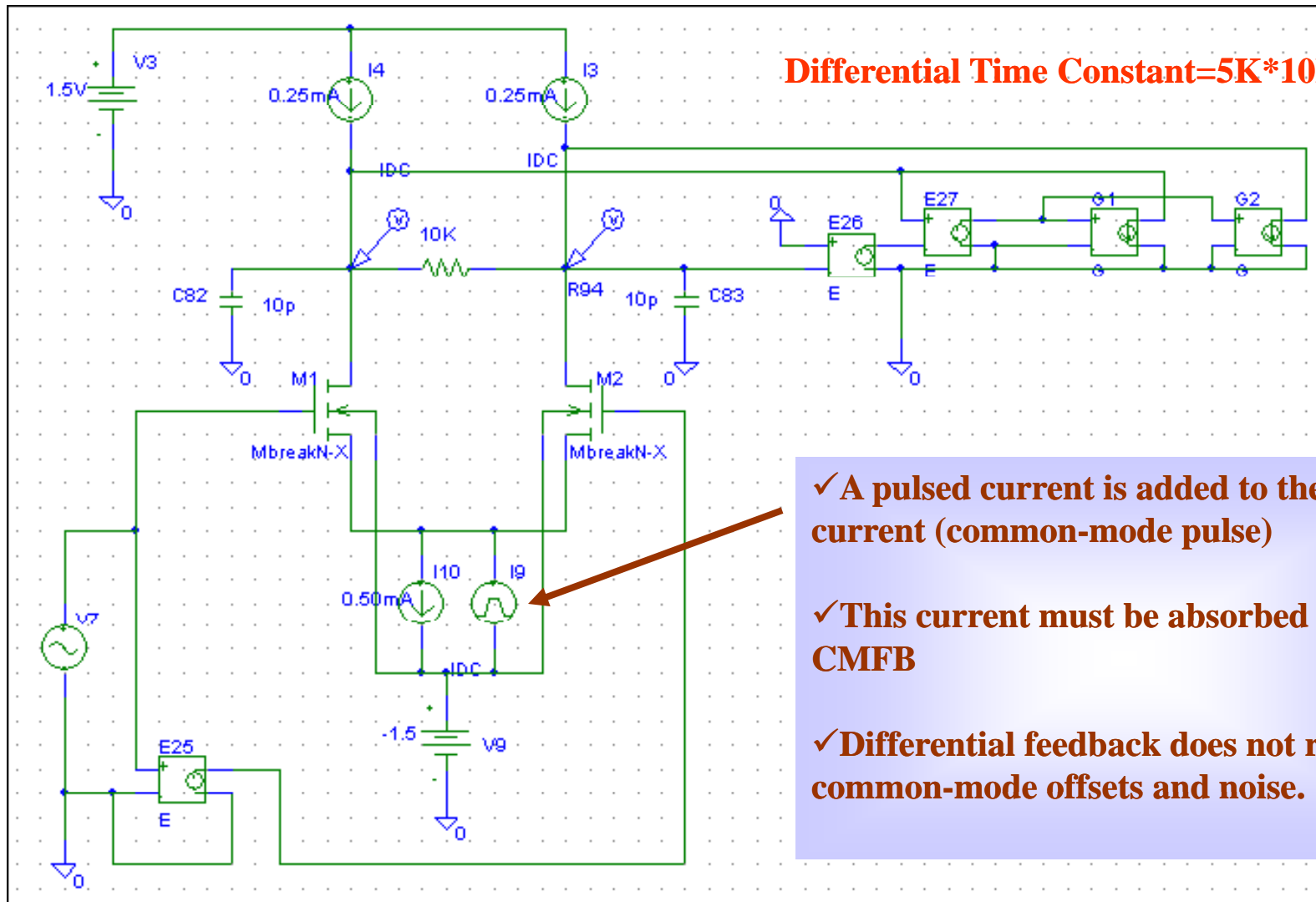




**Fig. 3 Common-mode feedback basic circuit concept. (a) Basic common-mode detector, (b) A CMOS CMFB Implementation.**

**Notice that the resistors  $R$  reduce the differential gain!**

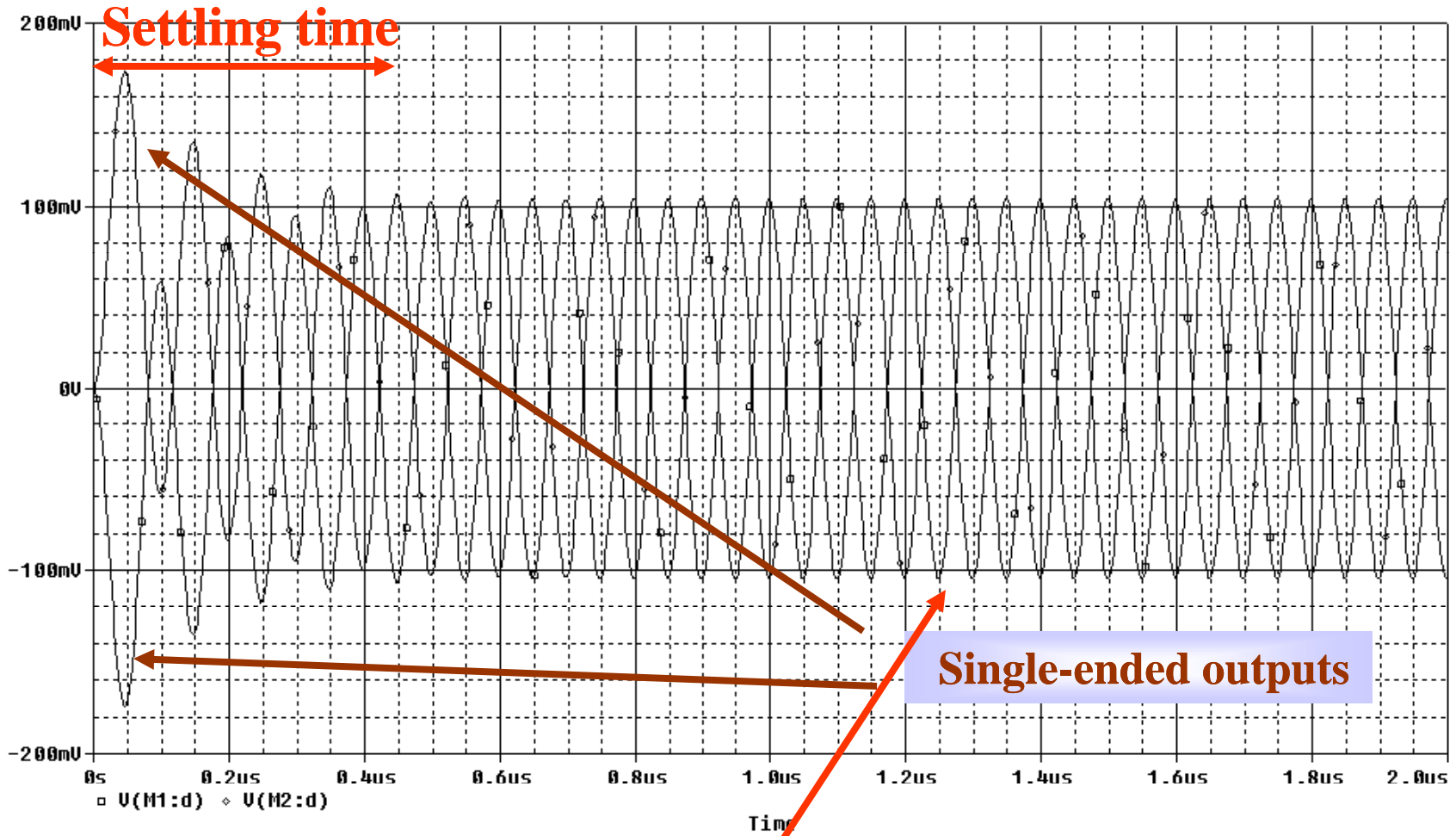
## Fully-Differential Amplifiers: Common-mode pulse



Differential Time Constant =  $5K * 10P = 50nsecs$

- ✓ A pulsed current is added to the tail current (common-mode pulse)
- ✓ This current must be absorbed by the CMFB
- ✓ Differential feedback does not reduce common-mode offsets and noise.

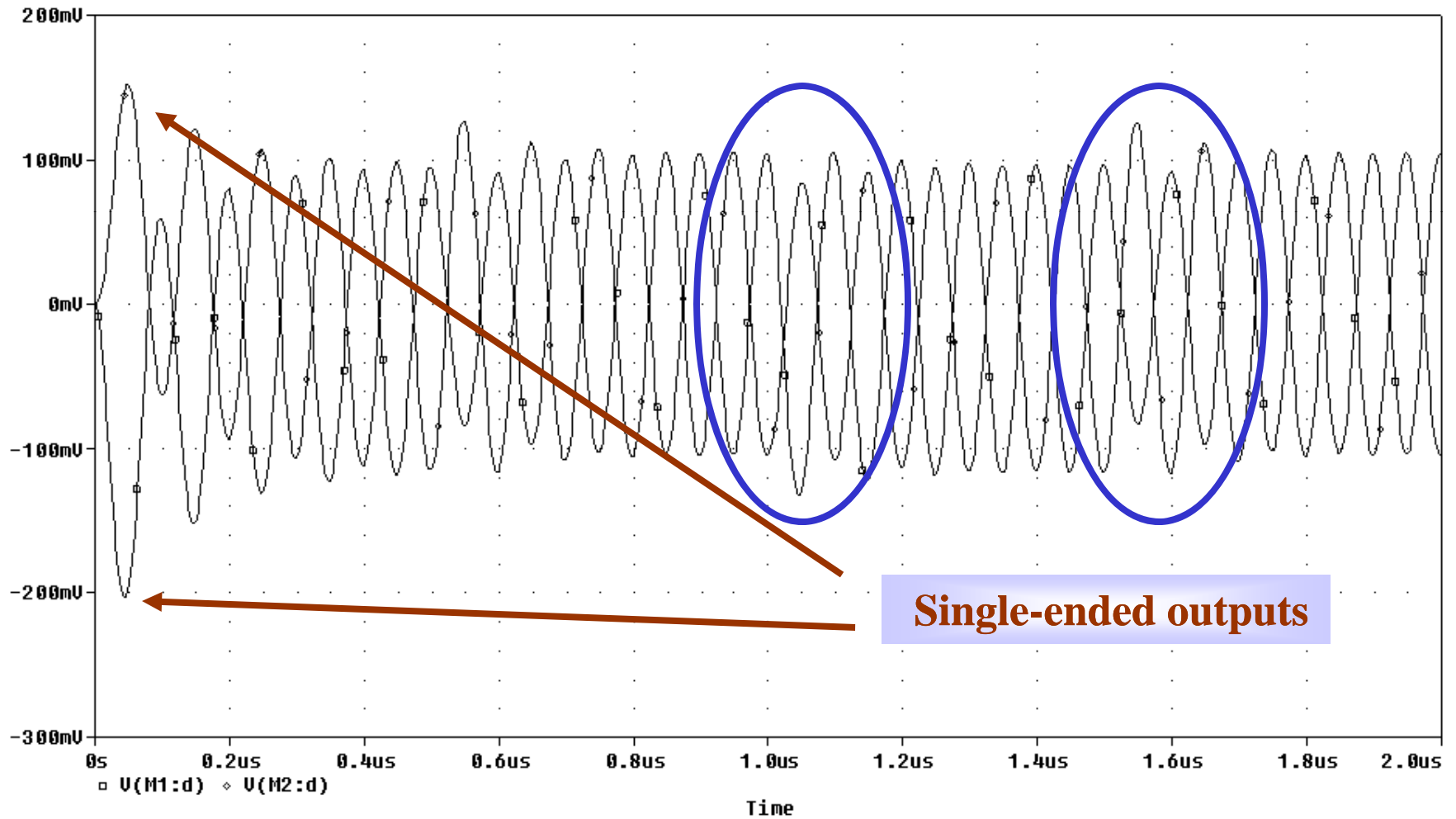
## Fully-Differential Amplifiers with CMFB Differential input signals only



Seems to be that the system is working fine, isn't it?

# Fully-Differential Amplifiers with CMFB

## Differential input signals + common-mode pulses

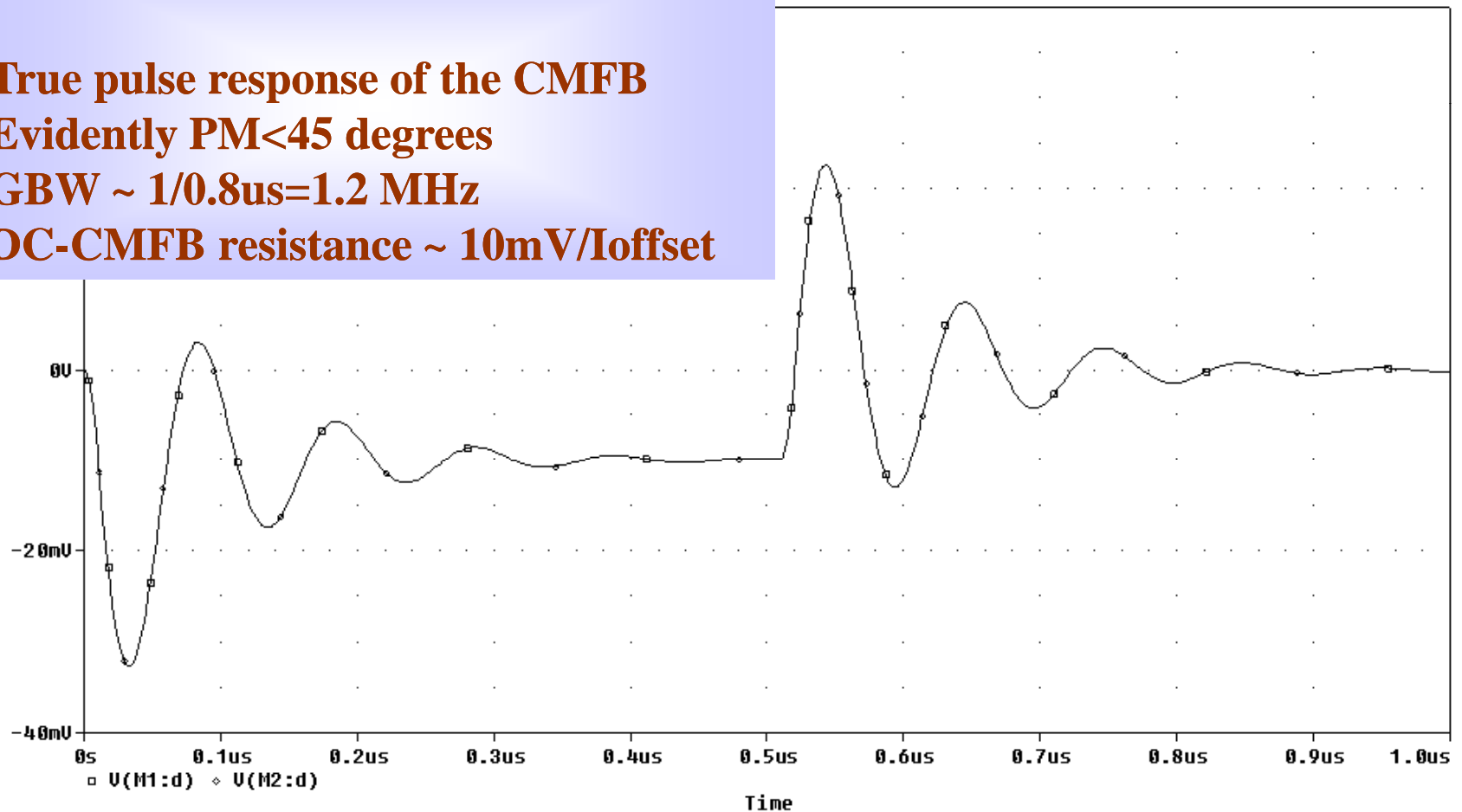


## Fully-Differential Amplifiers with CMFB

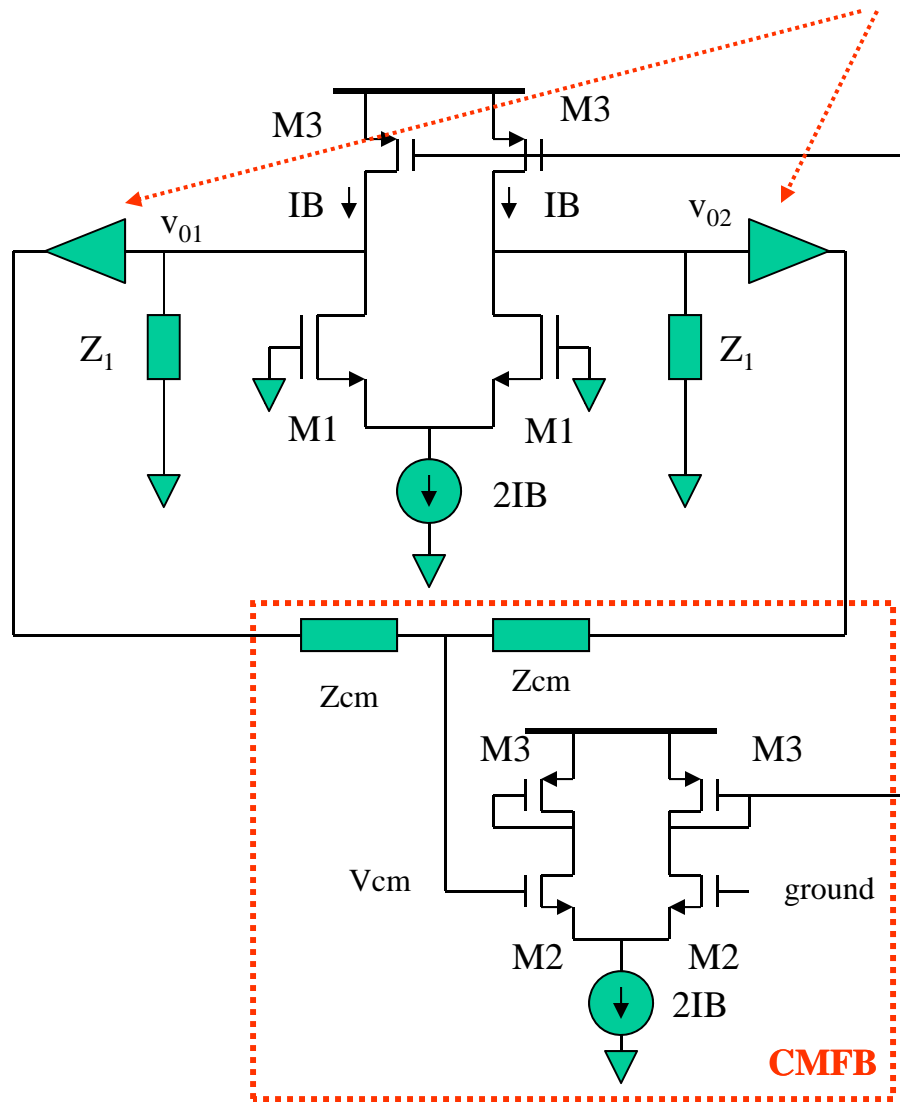
### Differential input signals + common-mode pulses

#### Common-mode output

True pulse response of the CMFB  
Evidently  $PM < 45$  degrees  
 $GBW \sim 1/0.8\mu s = 1.2$  MHz  
DC-CMFB resistance  $\sim 10$  mV/I<sub>offset</sub>

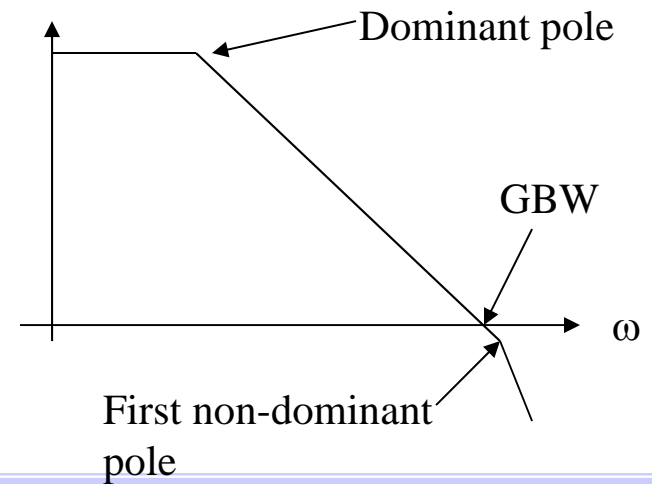


## Fully-Differential Filters: Adding buffers to handle the resistive CM-detector

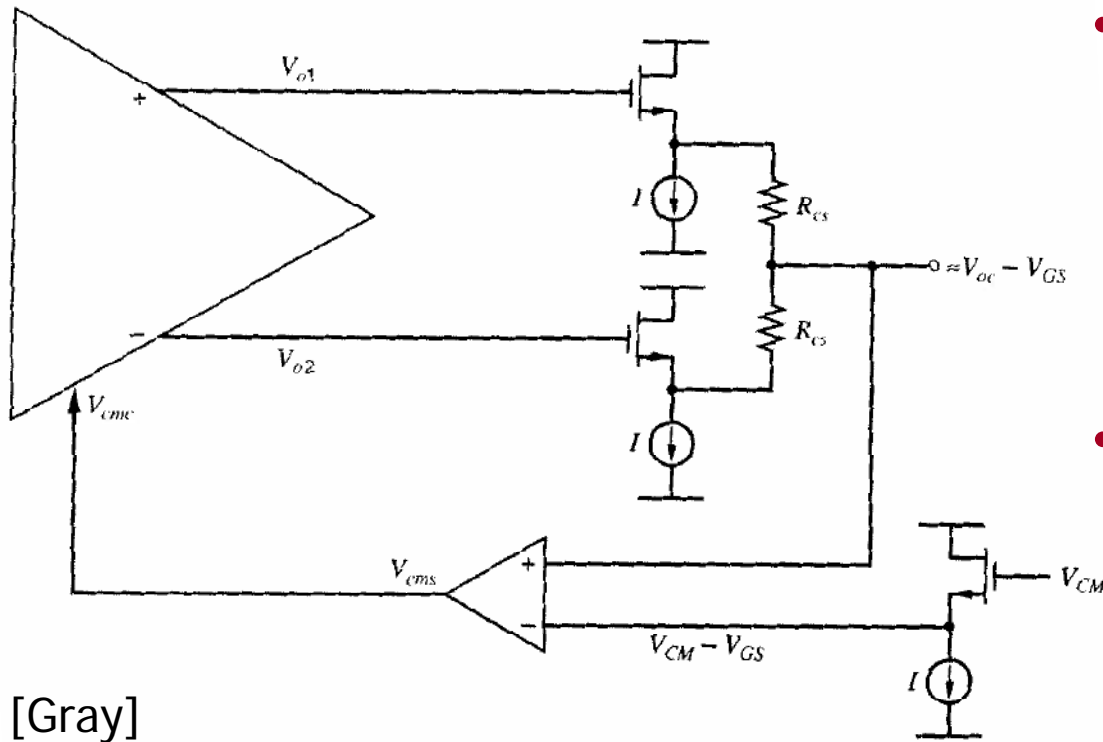


➤ The stability conditions are exactly the same for OTA's and OPAMP's:

- 1 pole at vcm ( $1/RC$ )
- 1 pole at gate of M3 ( $g_{m3}/C_{P3}$ )
- 1 pole at the output ( $g_{o1}/C_1$ )
- In OPAMP's you can use resistors as common-mode detector due to the presence of the output buffers
- dc gain =  $0.5g_{m2}R_{o1}$

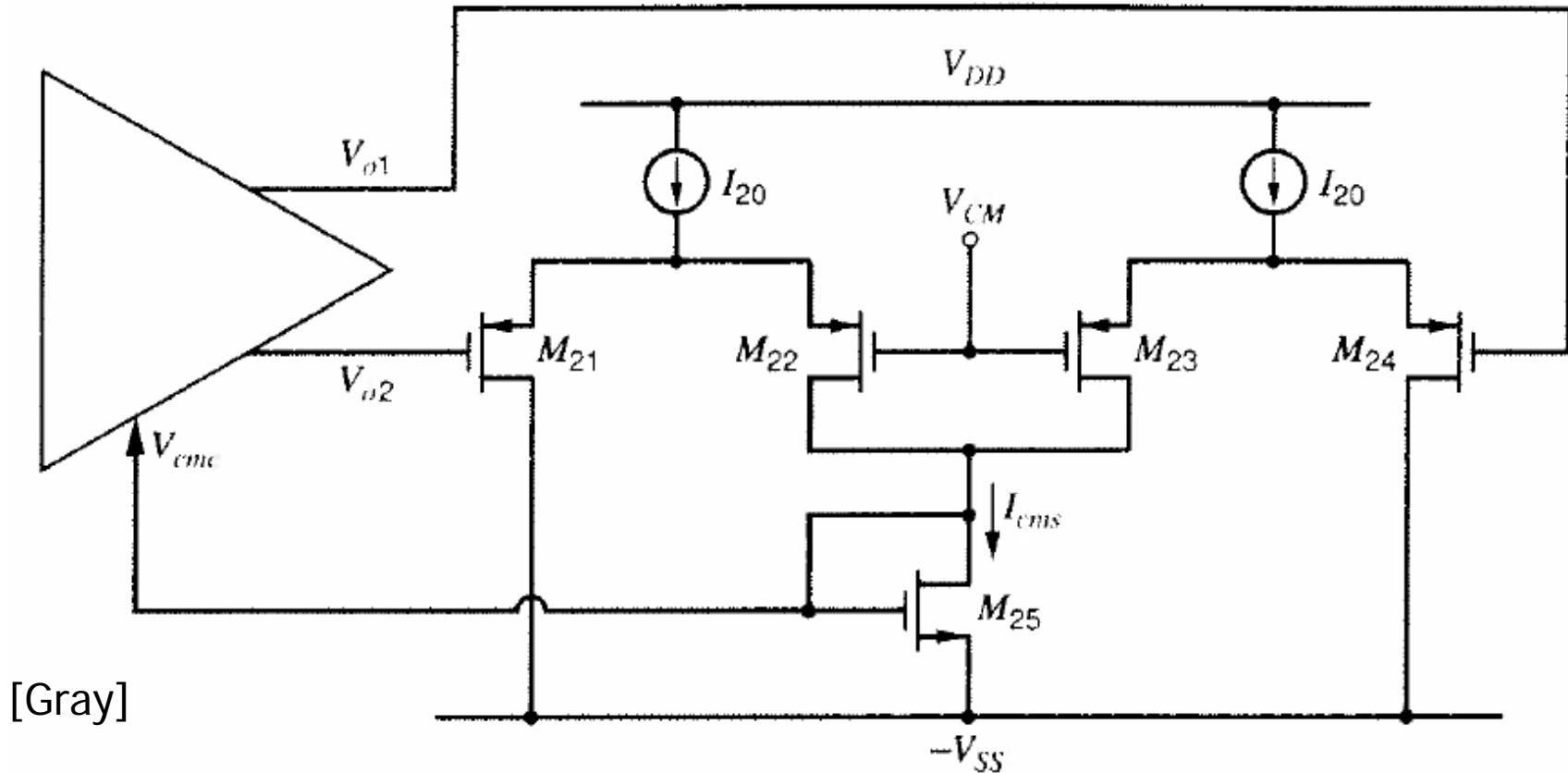


# Isolated Common-Mode Sensing



- Source-Followers isolate the loading of the common-mode sensor resistors
- Need to have a replica source follower to set the appropriate reference level for the CMFB amplifier

# Two Differential Pair CM Sensor



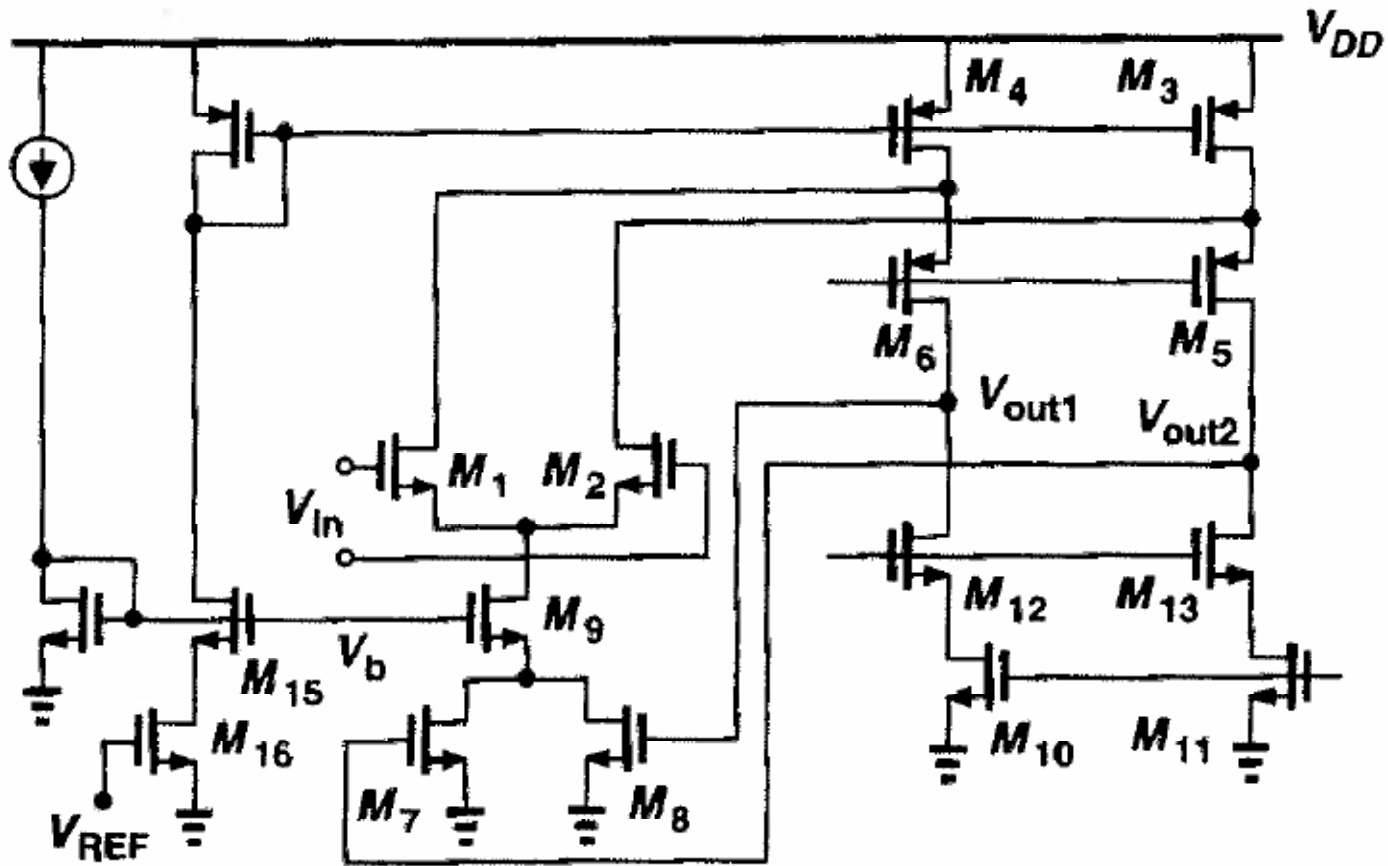
$$I_{cms} = I_{20} + g_{m22}(V_{oc} - V_{CM})$$

$$G_{cmf} = g_{m22}$$



# CMFB w/ Triode Devices in Tail Current Source

[Razavi]



# Next Time

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- Common-Mode Feedback Wrap-Up
- Variable Gain Amplifiers