

EXAM #2 ANALOG INTEGRATED FILTERS

This is a closed book (and notes) exam. You can only use a one page with information prepared by yourself. The total percentage (or in points) of this exam is 25.

Problem	Maximum	Yours
1	7	
2	6	
3	6	
4	6	
Extra Credit	1	
Total	26	

$$\text{REQUIRED } H_{\text{NOTCH}} = \frac{-(s^2 + \omega_0^2)}{s^2 + \frac{\omega_0}{Q}s + \omega_0^2} \quad (1)$$

Prob. 1. Given the following dead network,

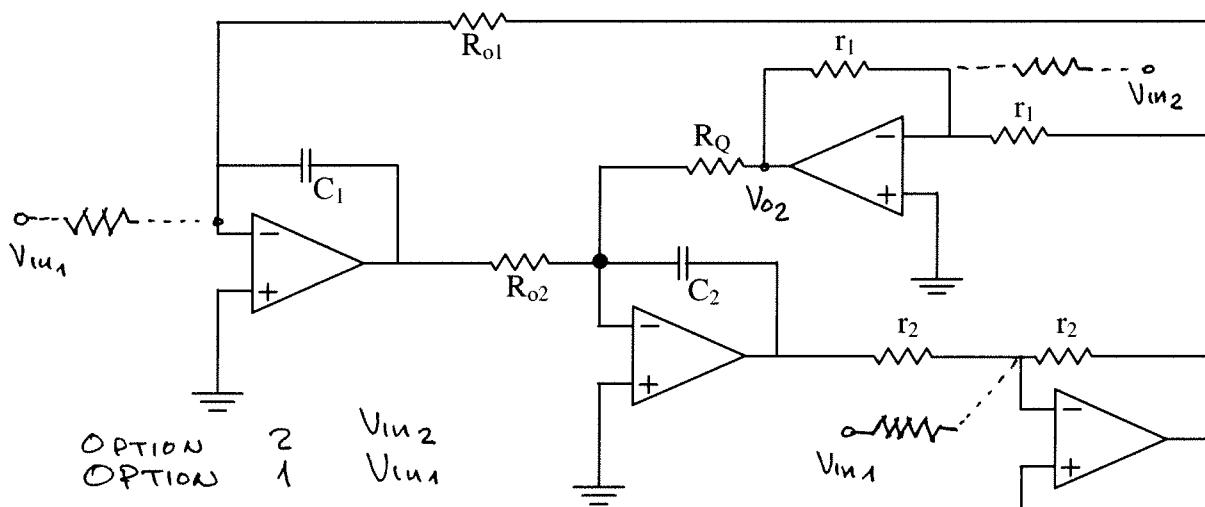
- a) Draw the input and output nodes yielding a notch (band elimination) filter.
add the minimum required components to obtain such a filter. *From Circuit*

- b) Draw the block diagram of the proposed notch filter.

$$D(s) = 1 + \frac{1}{sR_QC_2} + \frac{1}{s^2 R_Q C_2 C_1}$$

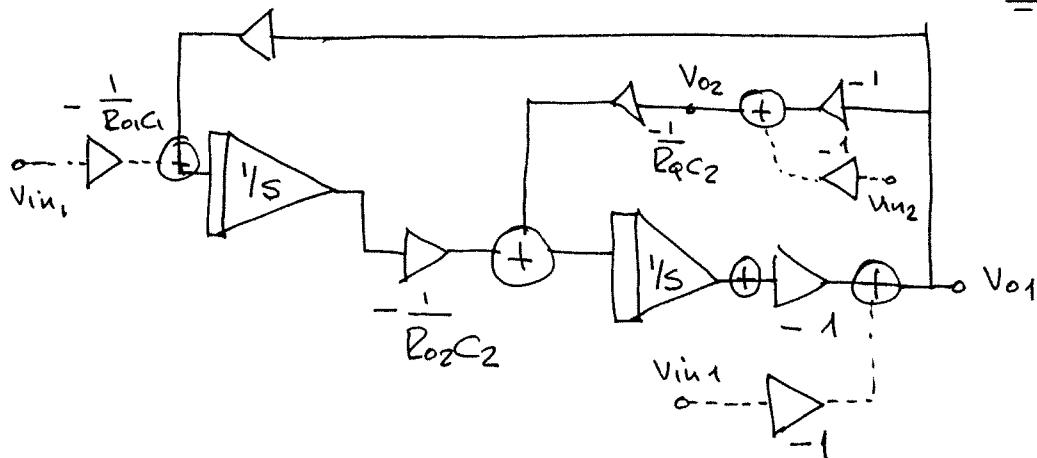
$$D(s) = \frac{1}{s^2} \left[s^2 + \frac{s}{R_Q C_2} + \frac{1}{R_Q C_2 C_1} \right]$$

*From (1) we
need both a
HP and a LP
components.*



OPTION 1
OPTION 2

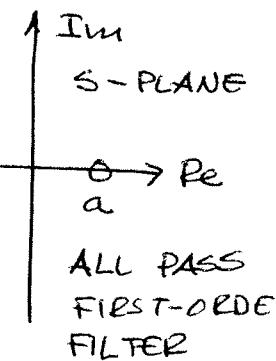
$$-\frac{1}{R_Q C_1}$$



*Note that for
option 2 the direct
path does not touch the
 ω_0^2 loop.*

Prob. 2. Obtain the corresponding $H(z)$ for

$$H(s) = \frac{a-s}{s+a} = -\frac{s-a}{s+a}$$

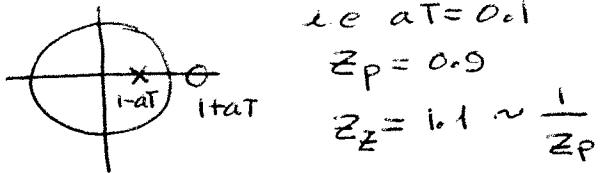


a) Assuming high sampling rate and identify the type of filter.

b) Using bilinear mapping

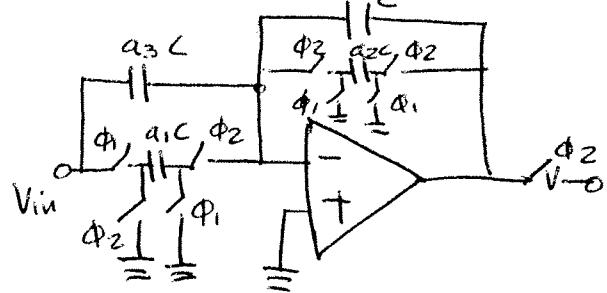
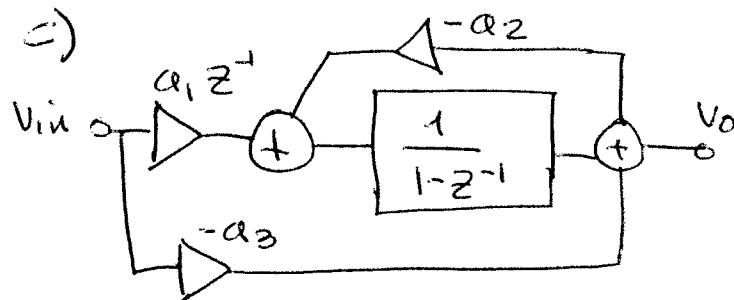
c) Propose a switched-capacitor implementation of $H(z)$ obtained in part b.

$$\text{a)} H(z) = H(s) \Big|_{\substack{s=\frac{z-1}{T} \\ z=\frac{z-1}{1+aT}}} = -\frac{z-(1+aT)}{z-(1-aT)}$$



$$\text{b)} H(z) \Big|_{\substack{s=c \\ s=\frac{z-1}{z+1}}} = H(s) \Big|_{\substack{s=c \\ z=\frac{z-1}{z+1}}} = -\frac{z-a'(z+1)-1}{z-1+a'(z+1)} = -\frac{1-a'}{1+a'} \frac{z-\frac{1+a'}{1-a'}}{z-\frac{1-a'}{1+a'}} ; \quad d = \frac{a}{c} = \frac{aT}{2}$$

$$H(z) = \frac{-1}{Z_0} \frac{z-z_0}{z-\frac{1}{Z_0}} ; \quad Z_0 = \frac{1+\frac{aT}{2}}{1-\frac{aT}{2}} ; \quad H(z) \Big|_{\substack{z=1 \\ w=0}} = 1 ; \quad H(z) \Big|_{\substack{z=-1 \\ w=2\pi f_c}} = 1$$



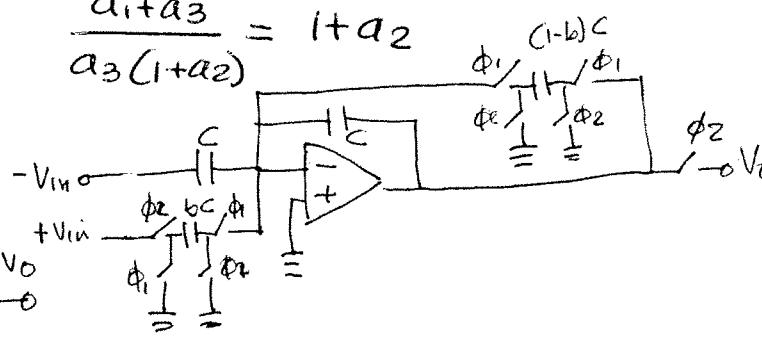
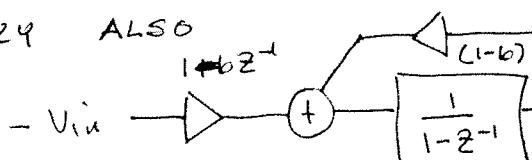
$$H(z) = -a_3 \frac{z - \frac{a_1 + a_3}{a_3(1+a_2)}}{z - \frac{1}{1+a_2}}$$

From b)

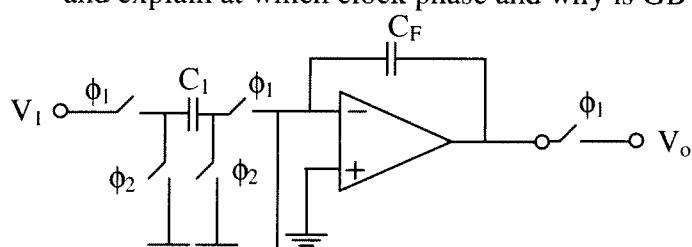
$$\frac{a_1 + a_3}{a_3(1+a_2)} = 1 + a_2$$

$$a_1 = a_2 a_3 (2 + a_2)$$

TRY ALSO



Prob. 3. a) Determine the expression for the required GB for a switched-capacitor filter operating at a clock frequency f_c . Assume $C_1 = C_2 = C_F$ and obtain the value of GB and explain at which clock phase and why is GB determined.



WORST CASE
DETERMINE
GB, FOR THIS
PROBLEM OCCURS
AT ϕ_1 .

$$\alpha_2 = \frac{C_F}{C_F} = 1$$

$$GBT > 5$$

$$GB > \frac{5x^2}{f_c} = 5f_c$$

$$\alpha = \frac{C_F}{C_F + C_1 + C_2}$$

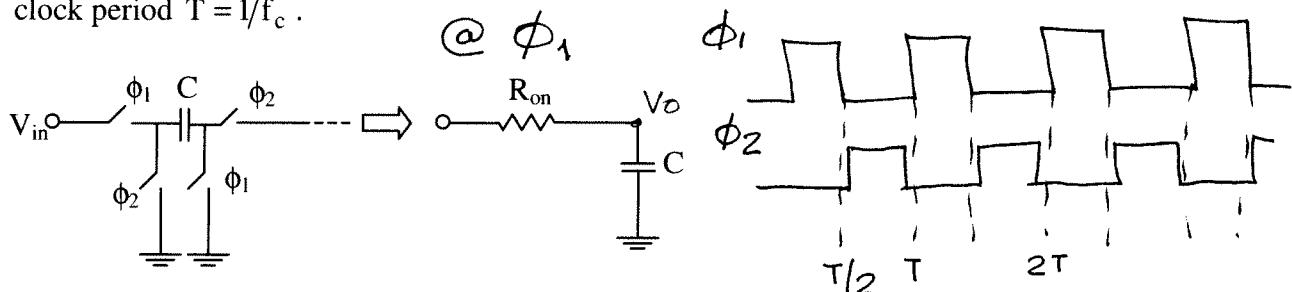
$$\alpha GB T_2 > 5$$

$$\text{FOR } C_F = C_1 = C_2$$

$$GB > 15 f_c \times 2$$

$$GB > 30 f_c$$

b) Assume that the switch, in a switched-capacitor circuit, when is on has a resistance of value R_{on} . Determine the optimal value of $R_{on} C$ as a function of the clock period $T = 1/f_c$.



$R_{on} C$ HAS TO BE CHARGED WITHIN $T/2$.

$$R_{on} C < 0.25T \text{ to } 0.5T$$

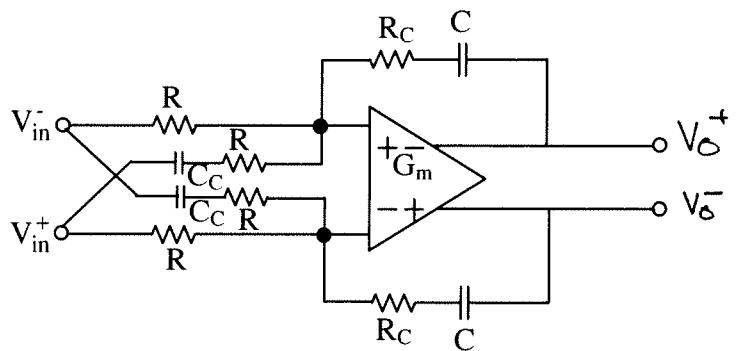
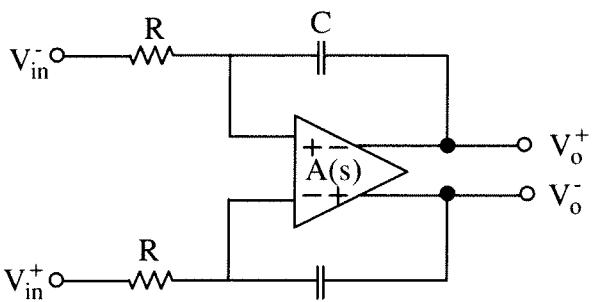
i.e.

$$k R_{on} C < \frac{T}{2} \quad R_{on} C < \frac{T}{2k} \quad k = 4 \text{ or } 5$$

$$R_{on} C < \frac{T}{10} = 0.1T \text{ or } \frac{T}{8} = 0.125T$$

$$V_o = V_{in} \left(1 - e^{-t/R_{on}C} \right) \Big|_{t=\frac{T}{2}}$$

Prob. 4. Assume an OTA is used instead of an op amp in a regular active-RC integrator. The transconductance G_m is given by $\frac{g_m}{(1+s/\omega_p)}$. In order to compensate the frequency effects of the OTA the circuit compensation shown in Fig. (b) is utilized. Determine the optimal values of C_C and R_C as functions of ω_p .



ORIGINAL TRANSFER FUNCTION IS UNCHANGED (a)

IF : $G_m = \frac{g_m}{1+s/\omega_p}$; $\frac{1}{R} \Rightarrow \frac{\frac{1}{R}}{1+s/\omega_p} = \frac{1}{R} - \frac{1}{R + \frac{\omega_p R}{s}}$

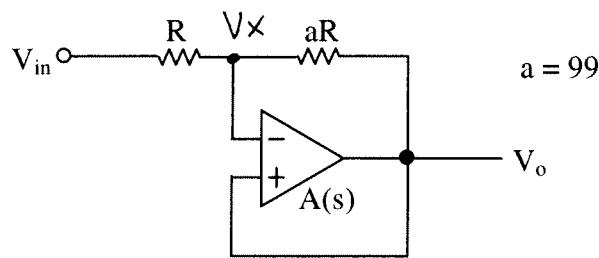
ORIGINAL COMPENSATION

$$sC \Rightarrow \frac{sC}{1+s/\omega_p} = \frac{1}{\frac{1}{sC} + \frac{1}{R + \frac{\omega_p R}{s}}} \text{, COMPENSATION}$$

THEREFORE C_C AND R_C CANCEL THE ω_p EFFECTS.

$$C_C = \frac{1}{\omega_p R} \quad \text{AND} \quad R_C = \frac{1}{\omega_p C}$$

Extra Credit (no partial credit). Explain how you could determine, in the lab, the value of the GB of an Op Amp using the circuit shown below and assuming that $A(s) \approx GB/S$.



$$a = 99$$

$$V_x \left(\frac{1}{R} + \frac{1}{aR} \right) - \frac{V_o}{aR} = \frac{V_{in}}{R} \quad (1)$$

$$V_o = (V_o - V_x)A \quad (2)$$

FROM (2)

$$V_o(1-A) = -AV_x$$

$$V_x = \frac{V_o(A-1)}{A} \quad (2')$$

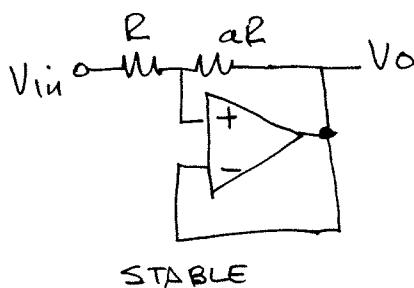
(2') INTO (1)

$$\frac{V_o(A-1)}{A} \left(\frac{1}{R} + \frac{1}{aR} \right) - \frac{V_o}{aR} = \frac{V_{in}}{R}$$

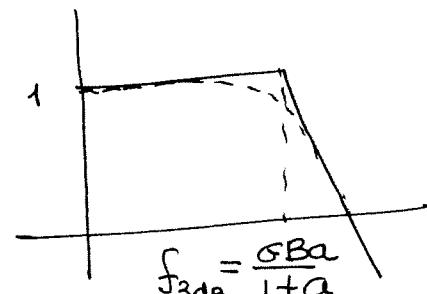
$$V_o \left[\left(1 - \frac{1}{A} \right) \left(1 + \frac{1}{a} \right) - \frac{1}{a} \right] = V_{in} = \left[1 + \cancel{\frac{1}{a}} - \frac{1}{A} - \frac{1}{Aa} - \cancel{\frac{1}{a}} \right] V_o$$

$$\frac{V_o}{V_{in}} = \frac{1}{1 - \frac{1}{A} \left(1 + \frac{1}{a} \right)} \quad \left| \begin{array}{l} \\ \\ A = \frac{GB}{S} \end{array} \right. = \frac{1}{1 - \frac{S}{GB} \left(1 + \frac{1}{a} \right)}$$

UNSTABLE



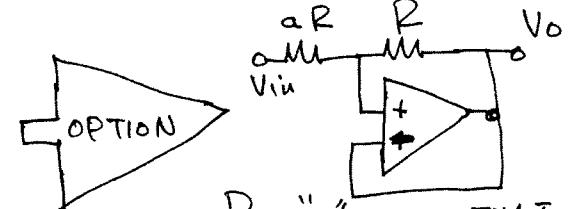
$$\frac{V_o}{V_{in}} = \frac{1}{1 + \frac{S}{GB} \left(1 + \frac{1}{a} \right)}$$



$$f_{3dB} \approx GB \frac{99}{100} \approx GB$$

If you can sweep f_{3dB} by changing a
i.e. $a = 9 \Rightarrow f_{3dB} = 0.9 \text{ GB}$

$$a = \frac{1}{99} \Rightarrow f_{3dB} = \frac{GB}{100}$$



Pick "a" such that
is measured at