

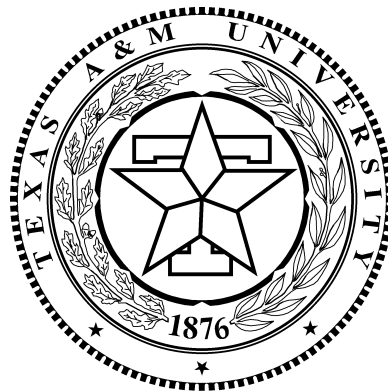
ECEN 326

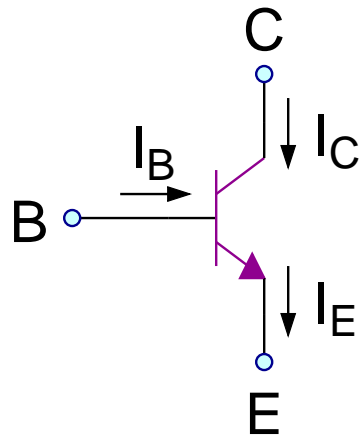
Electronic Circuits

Introduction

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Department of Electrical and Computer Engineering



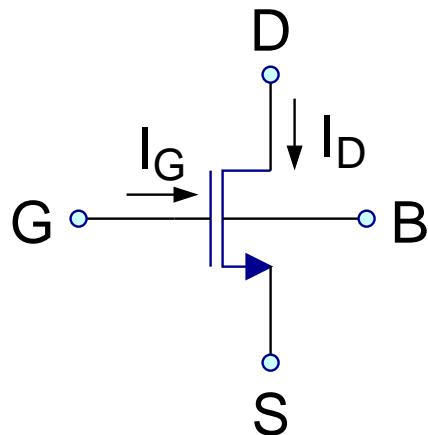


$$V_{CE} \geq V_{CE,sat} \Rightarrow \text{ACTIVE}$$

$$V_{BE} = 0.7 \text{ V}$$

$$I_C = \beta I_B$$

$$I_E = I_C + I_B$$

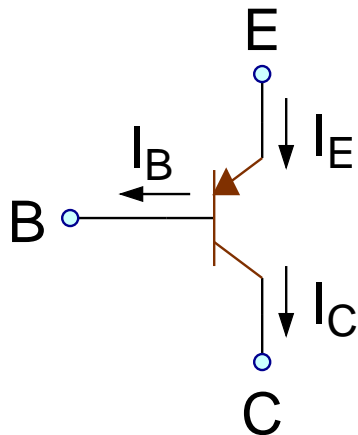


$$V_{DS} \geq V_{ov} \Rightarrow \text{ACTIVE}$$

$$V_{ov} = V_{GS} - V_{tn}$$

$$I_G = 0$$

$$I_D = \frac{k'_n}{2} \frac{W}{L} V_{ov}^2$$

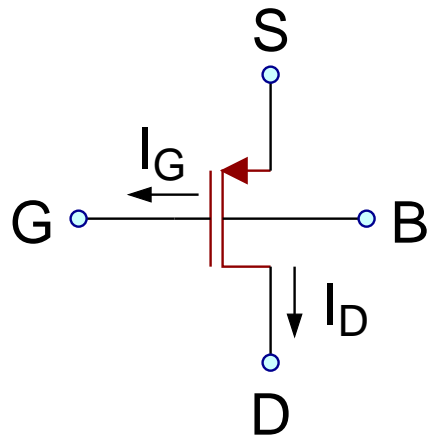


$$V_{EC} \geq V_{EC,sat} \Rightarrow \text{ACTIVE}$$

$$V_{EB} = 0.7 \text{ V}$$

$$I_C = \beta I_B$$

$$I_E = I_C + I_B$$



$$V_{SD} \geq V_{ov} \Rightarrow \text{ACTIVE}$$

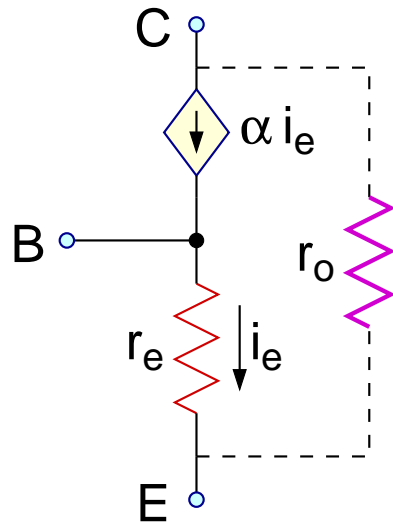
$$V_{ov} = V_{SG} - |V_{tp}|$$

$$I_G = 0$$

$$I_D = \frac{k'_p}{2} \frac{W}{L} V_{ov}^2$$

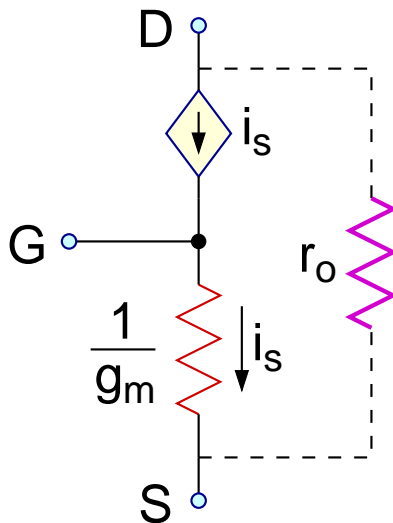
NPN & NMOS

Small-signal T model, $r_o = \infty$



$$r_e = \frac{V_T}{I_E} = \frac{\alpha}{g_m} \approx \frac{1}{g_m}$$

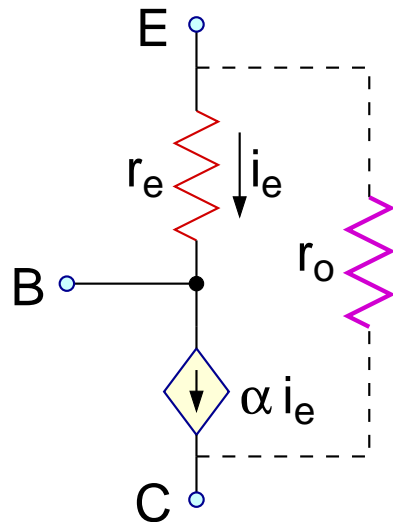
$$g_m = \frac{I_C}{V_T}$$



$$g_m = k'_n \frac{W}{L} V_{ov} = \sqrt{2k'_n \frac{W}{L} I_D}$$

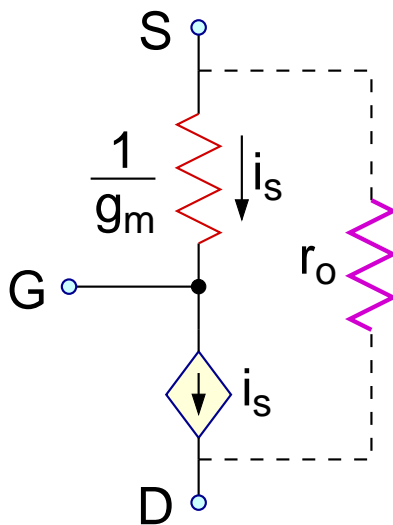
PNP & PMOS

Small-signal T model, $r_o = \infty$



$$r_e = \frac{V_T}{I_E} = \frac{\alpha}{g_m} \approx \frac{1}{g_m}$$

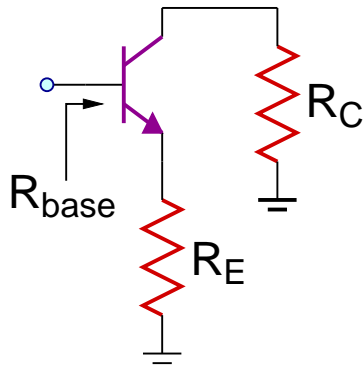
$$g_m = \frac{I_C}{V_T}$$



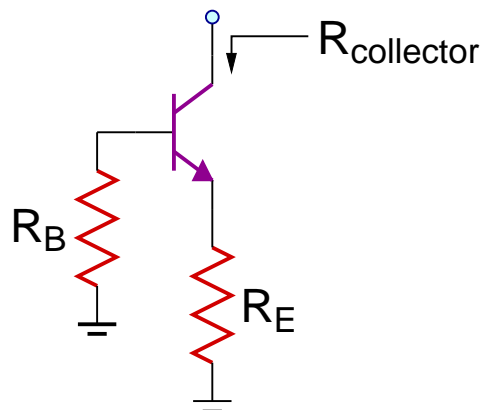
$$g_m = k'_p \frac{W}{L} V_{ov} = \sqrt{2k'_p \frac{W}{L} I_D}$$

BJT Node Resistances

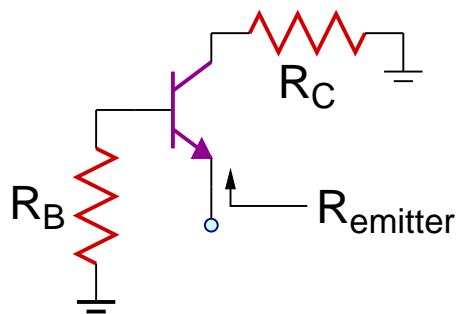
AC, $r_o = \infty$



$$R_{base} = (\beta + 1)(r_e + R_E)$$



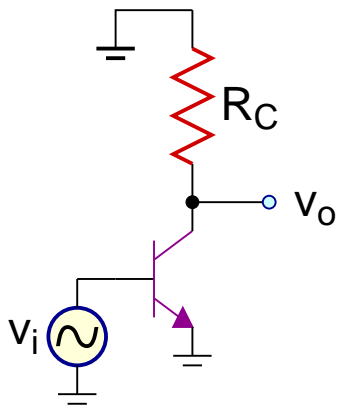
$$R_{collector} = \infty$$



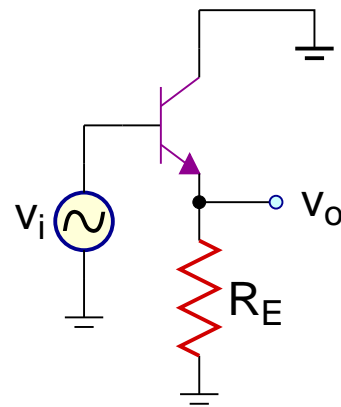
$$R_{emitter} = r_e + \frac{R_B}{\beta + 1}$$

BJT Amplifiers

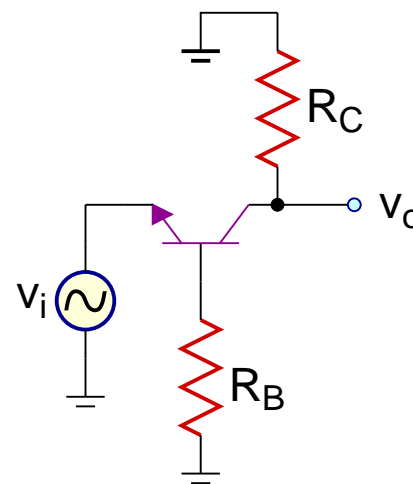
AC, $r_o = \infty$



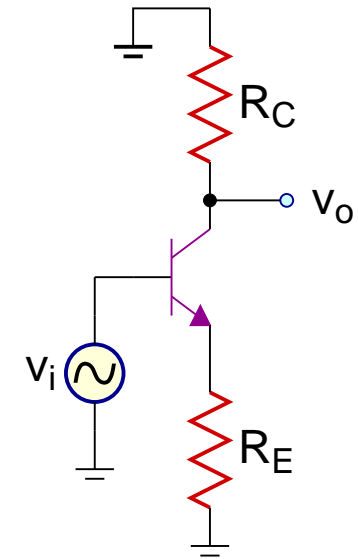
$$\frac{v_o}{v_i} = \frac{-\alpha R_C}{r_e}$$



$$\frac{v_o}{v_i} = \frac{R_E}{r_e + R_E}$$



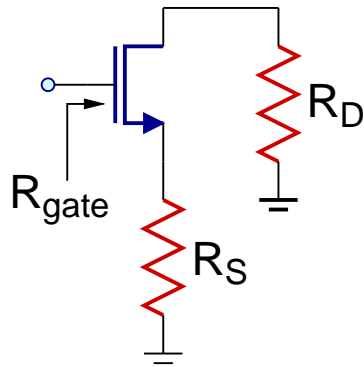
$$\frac{v_o}{v_i} = \frac{\alpha R_C}{R_{emitter}}$$



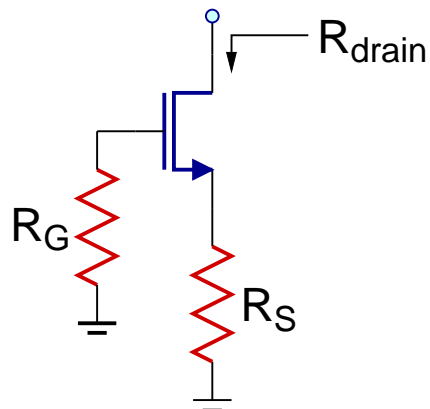
$$\frac{v_o}{v_i} = \frac{-\alpha R_C}{r_e + R_E}$$

MOS Node Resistances

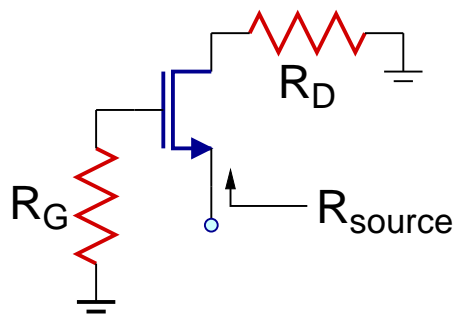
AC, $r_o = \infty$



$$R_{gate} = \infty$$



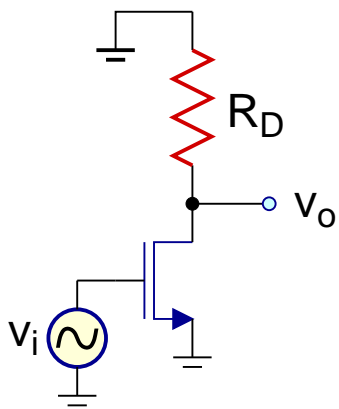
$$R_{drain} = \infty$$



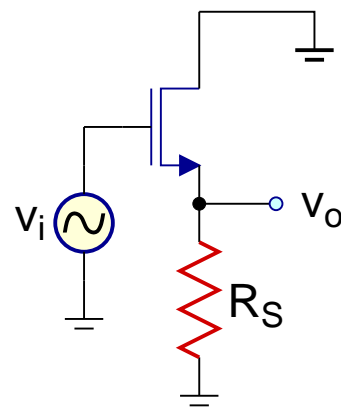
$$R_{source} = \frac{1}{g_m}$$

MOS Amplifiers

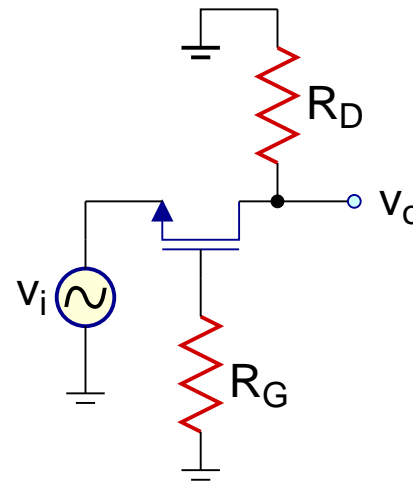
AC, $r_o = \infty$



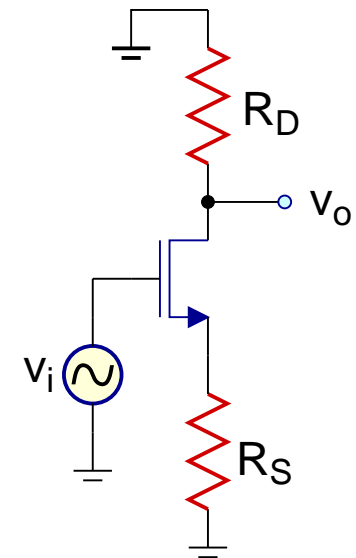
$$\frac{v_o}{v_i} = \frac{-R_D}{\frac{1}{g_m}}$$



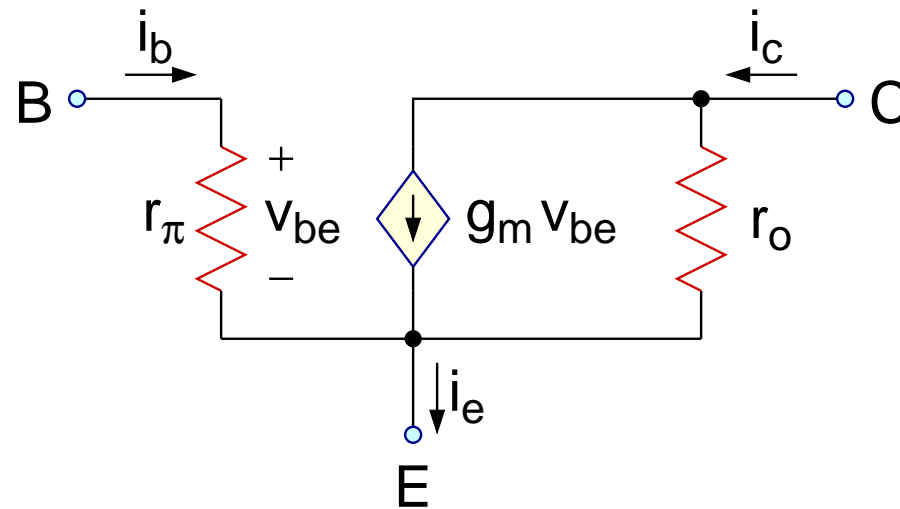
$$\frac{v_o}{v_i} = \frac{R_S}{\frac{1}{g_m} + R_S}$$



$$\frac{v_o}{v_i} = \frac{R_D}{R_{\text{source}}}$$



$$\frac{v_o}{v_i} = \frac{-R_D}{\frac{1}{g_m} + R_S}$$



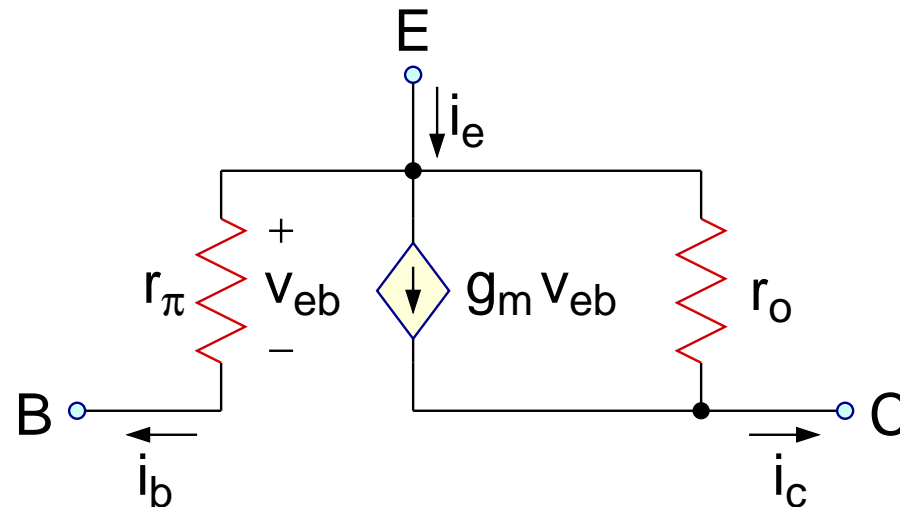
Early Effect $\rightarrow r_o$

$$g_m = \frac{I_C}{V_T}$$

$$r_o = \frac{V_A}{I_C}$$

$$r_\pi = \frac{\beta}{g_m}$$

$$V_T = \frac{kT}{q}$$



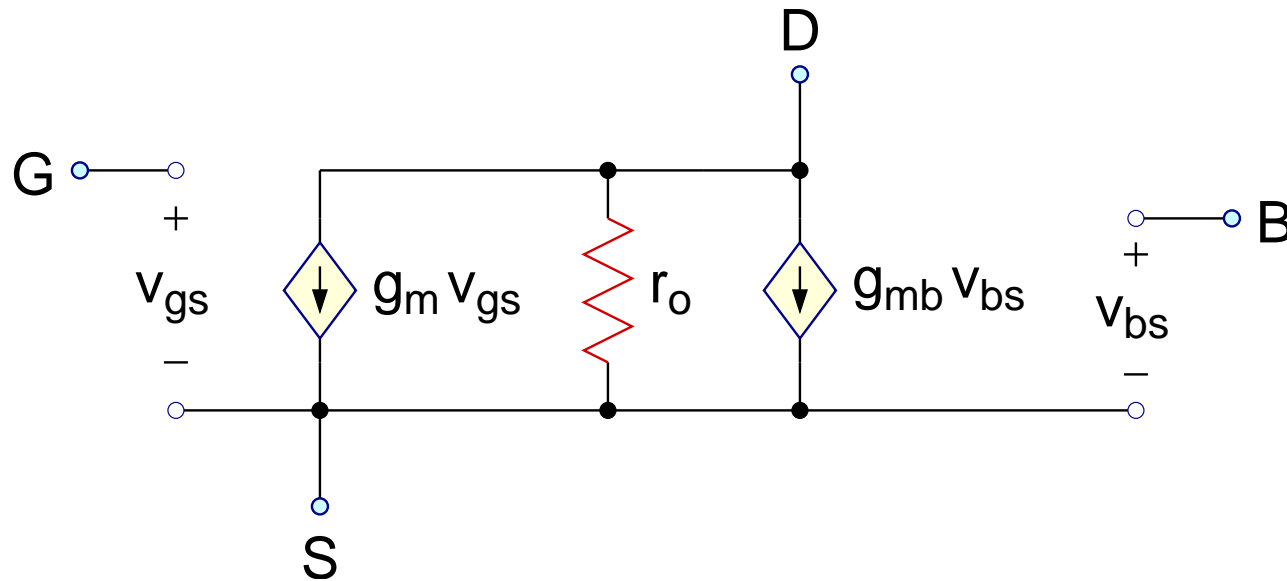
Early Effect $\rightarrow r_o$

$$g_m = \frac{I_C}{V_T}$$

$$r_o = \frac{V_A}{I_C}$$

$$r_\pi = \frac{\beta}{g_m}$$

$$V_T = \frac{kT}{q}$$



Channel Length Modulation $\rightarrow r_o$

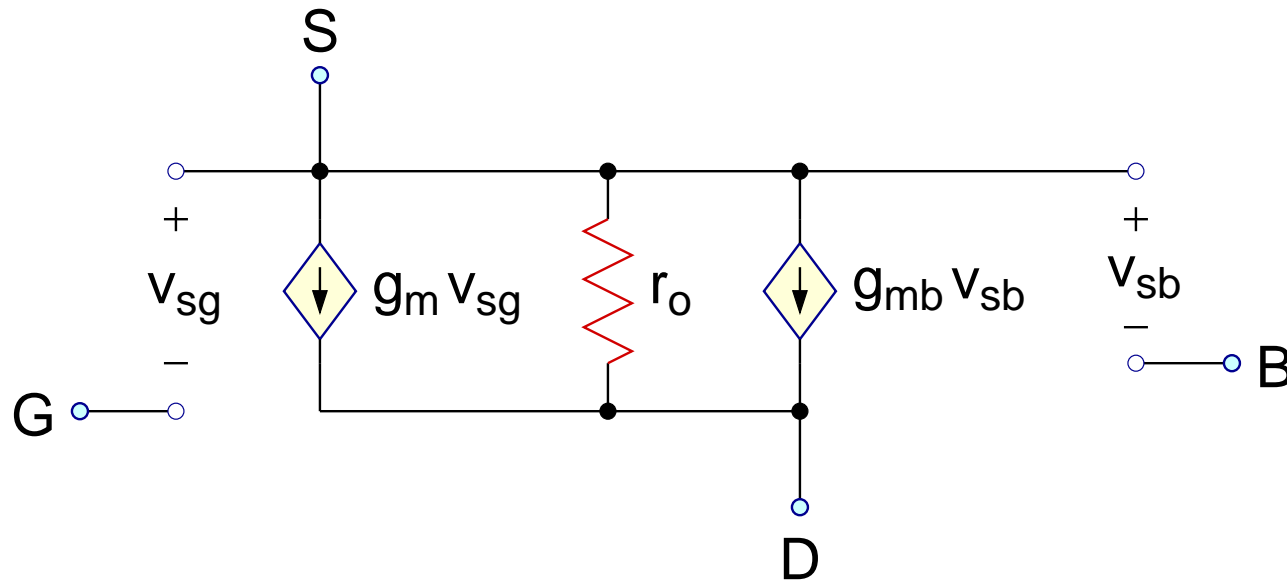
Body Effect ($V_t = V_{t0} + \gamma [\sqrt{|-2\phi_F + V_{SB}|} - \sqrt{|-2\phi_F|}]$) $\rightarrow g_{mb}$

$$g_m = \sqrt{2k'_n \frac{W}{L} I_D}$$

$$r_o = \frac{1}{\lambda_n I_D}$$

$$g_{mb} = \chi g_m$$

$$k'_n = \mu_n C_{ox}$$



Channel Length Modulation $\rightarrow r_o$

Body Effect ($V_t = V_{t0} + \gamma [\sqrt{|-2\phi_F + V_{SB}|} - \sqrt{|-2\phi_F|}]$) $\rightarrow g_{mb}$

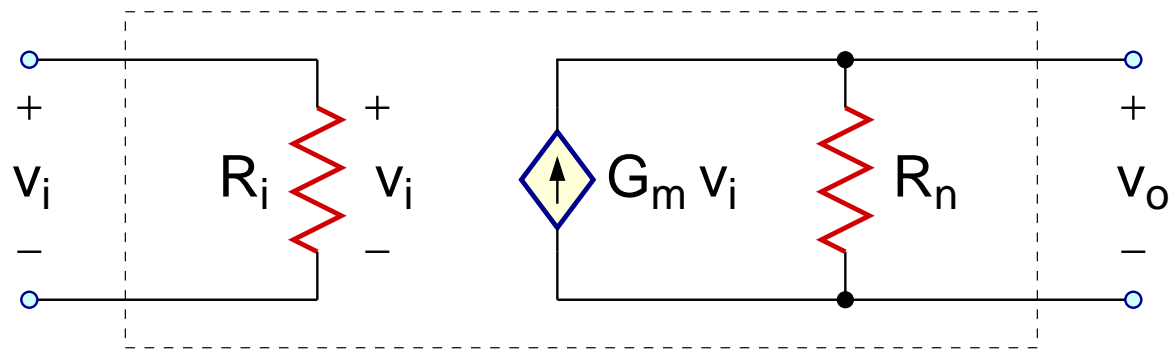
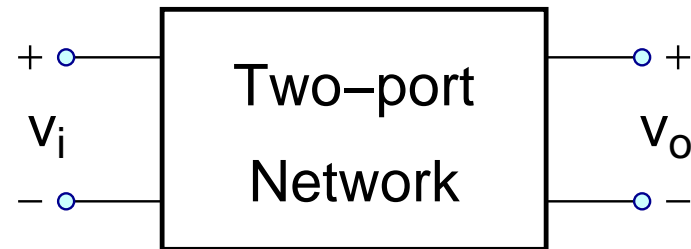
$$g_m = \sqrt{2k'_p \frac{W}{L} I_D}$$

$$r_o = \frac{1}{\lambda_p I_D}$$

$$g_{mb} = \chi g_m$$

$$k'_p = \mu_p C_{ox}$$

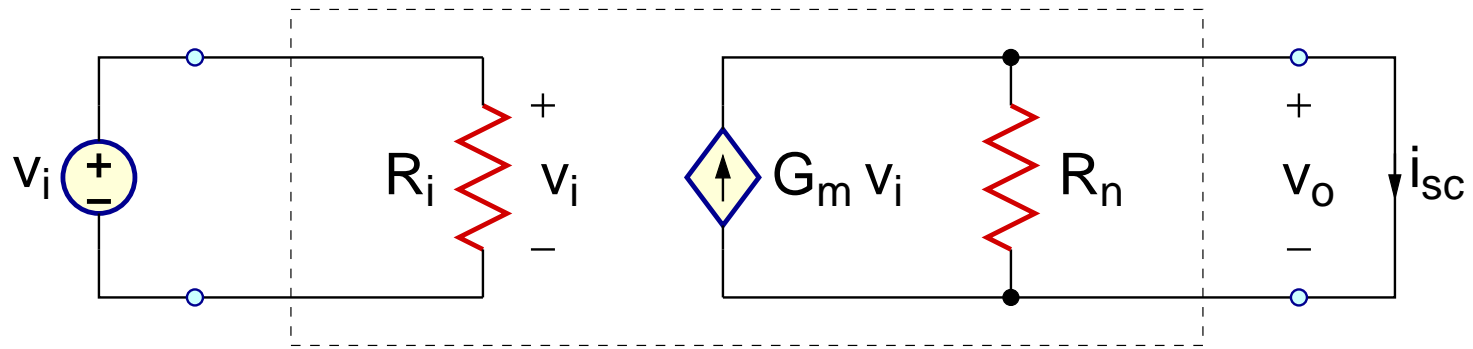
Two-Port Modeling of Amplifiers



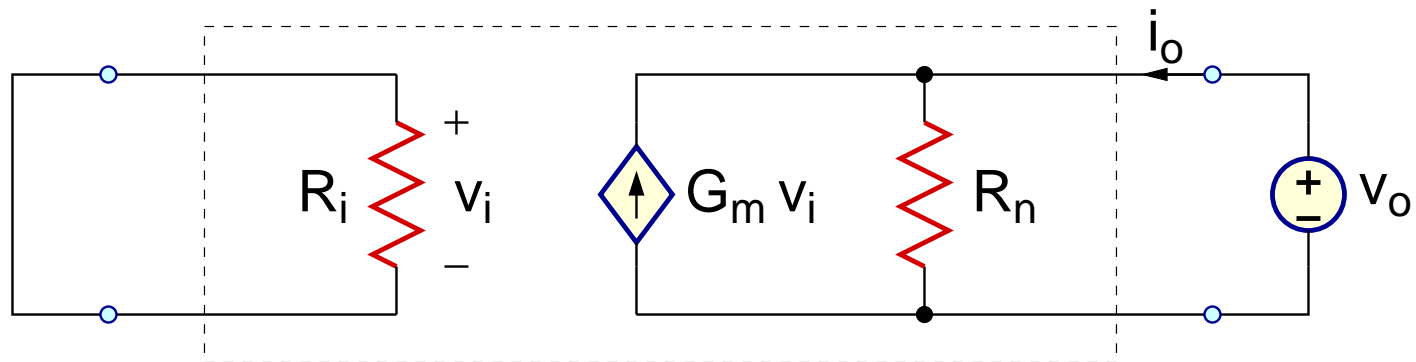
$$\frac{V_o}{V_i} = G_m R_n$$

Two-Port Modeling of Amplifiers

G_m & R_n



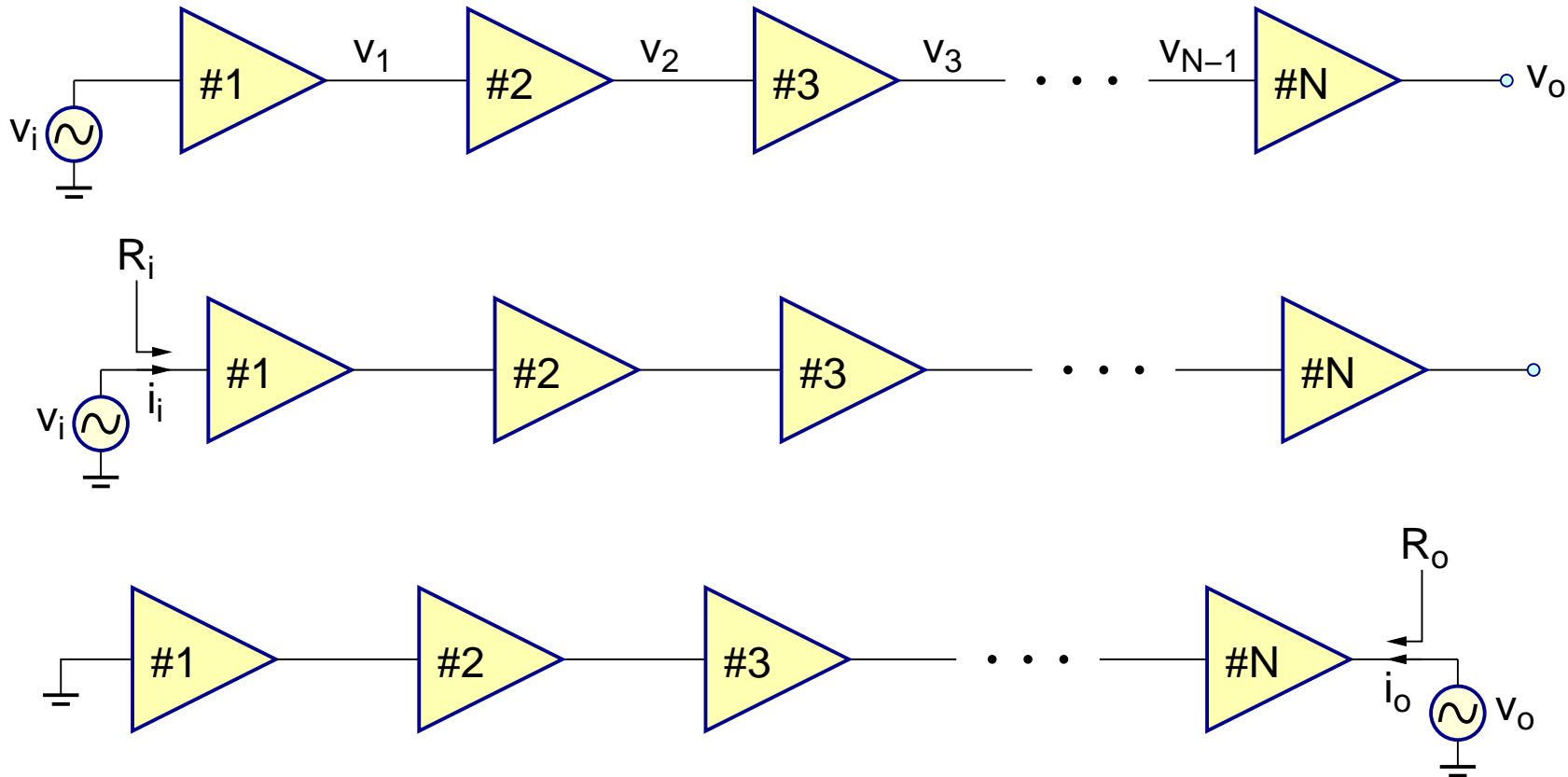
$$G_m = \frac{i_{sc}}{v_i} \Big|_{v_o=0}$$



$$R_n = \frac{v_o}{i_o} \Big|_{v_i=0}$$

Two-Port Modeling of Amplifiers

Multistage



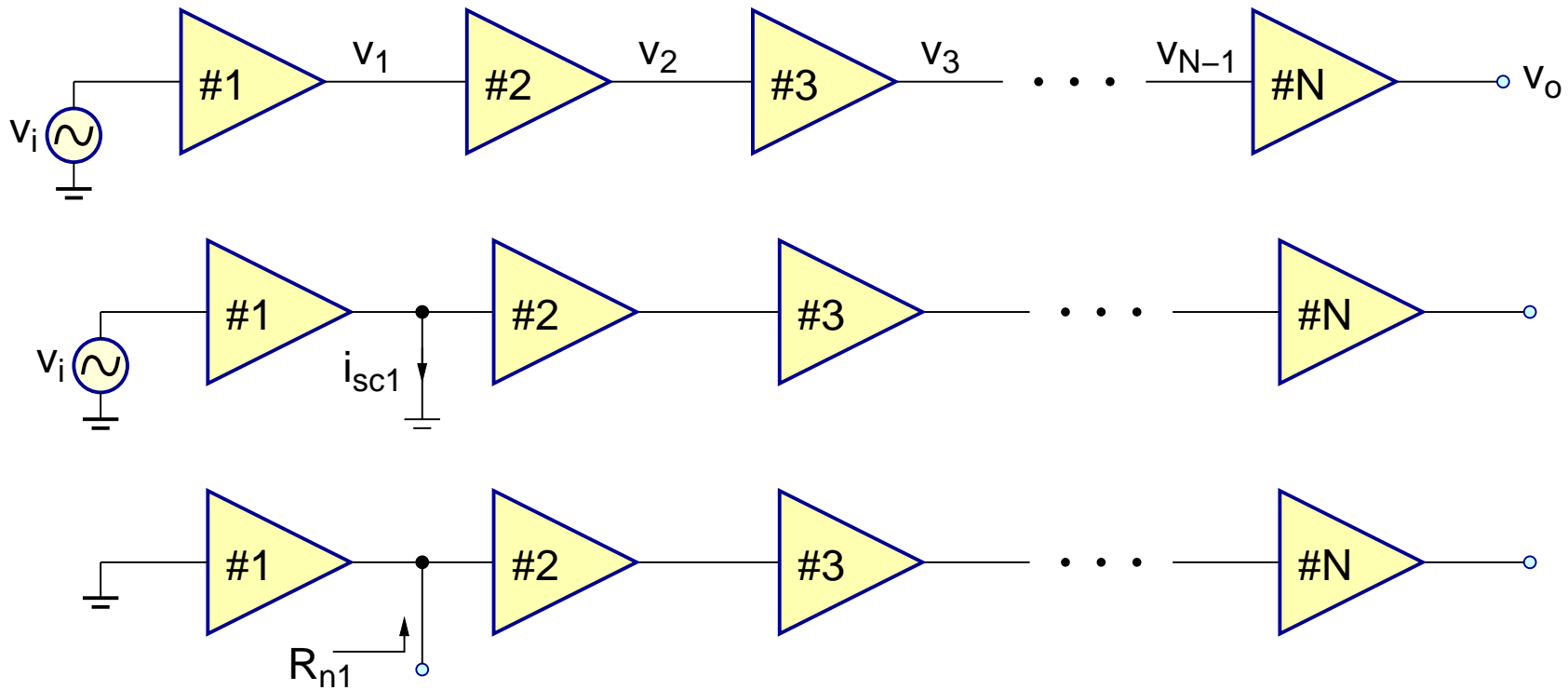
$$\frac{V_o}{V_i} = \frac{V_1}{V_i} \frac{V_2}{V_1} \dots \frac{V_o}{V_{N-1}}$$

$$R_i = \frac{V_i}{i_i}$$

$$R_o = \frac{V_o}{i_o}$$

Two-Port Modeling of Amplifiers

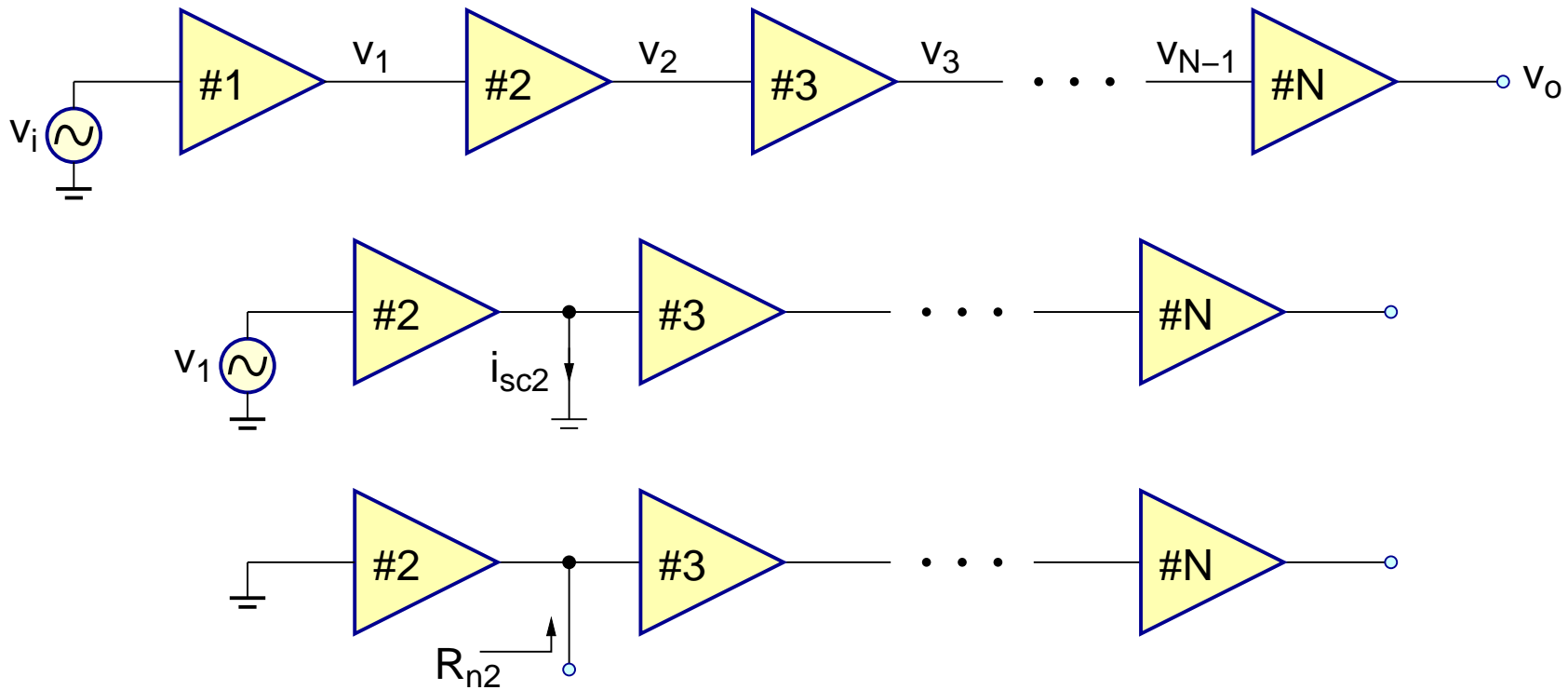
Multistage



$$G_{m1} = \frac{i_{sc1}}{v_i} \quad \frac{v_1}{v_i} = G_{m1}R_{n1}$$

Two-Port Modeling of Amplifiers

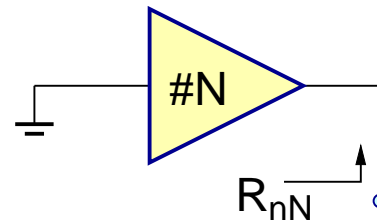
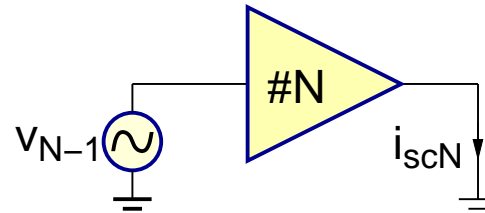
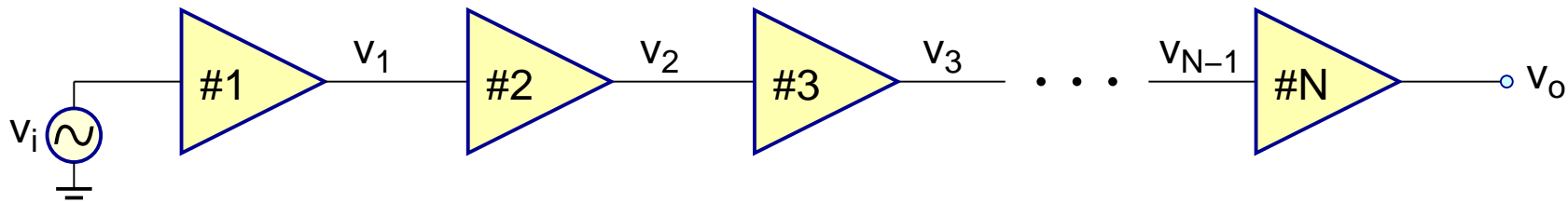
Multistage



$$G_{m2} = \frac{i_{sc2}}{v_1} \quad \frac{v_2}{v_1} = G_{m2}R_{n2}$$

Two-Port Modeling of Amplifiers

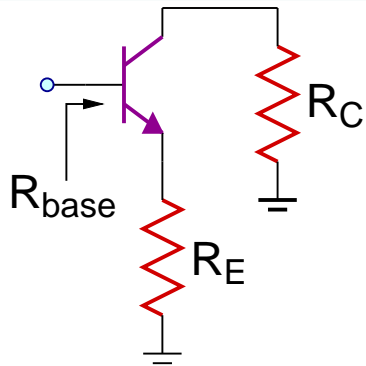
Multistage



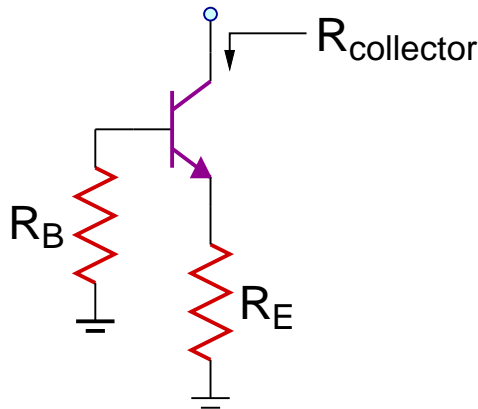
$$G_{mN} = \frac{i_{scN}}{v_{N-1}} \quad \frac{v_o}{v_{N-1}} = G_{mN} R_{nN}$$

BJT Node Resistances

AC

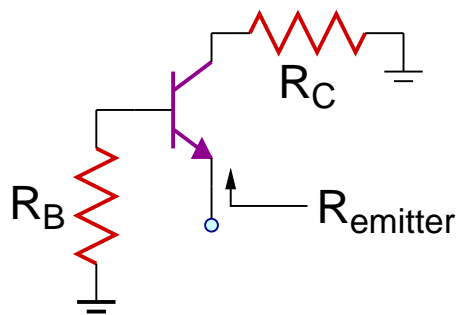


$$R_{\text{base}} = r_{\pi} + (\beta + 1)R_E \frac{r_o + \frac{R_C}{\beta + 1}}{r_o + R_C + R_E}$$



$$R_{\text{collector}} = g'_m r_o R_x + r_o + R_x$$

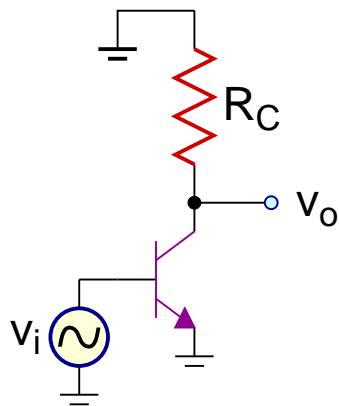
$$g'_m = g_m \frac{r_{\pi}}{r_{\pi} + R_B}, \quad R_x = R_E \parallel (r_{\pi} + R_B)$$



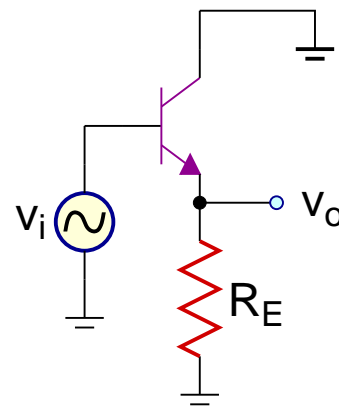
$$R_{\text{emitter}} = (r_{\pi} + R_B) \parallel \left[\left(\frac{1}{g'_m} \parallel r_o \right) \left(1 + \frac{R_C}{r_o} \right) \right]$$

$$g'_m = g_m \frac{r_{\pi}}{r_{\pi} + R_B}$$

Calculation of $\mathbf{G_m}$ and $\mathbf{R_n}$ is not necessary if $\mathbf{r_o}$ is grounded, since it can be combined with either $\mathbf{R_E}$ or $\mathbf{R_C}$.



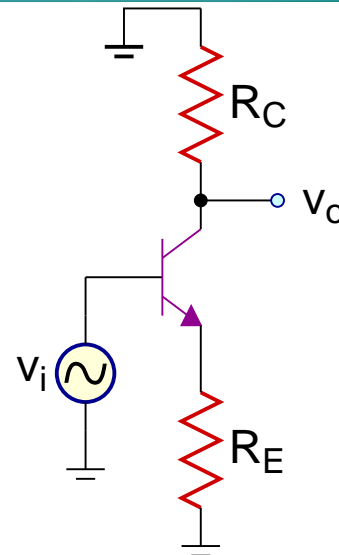
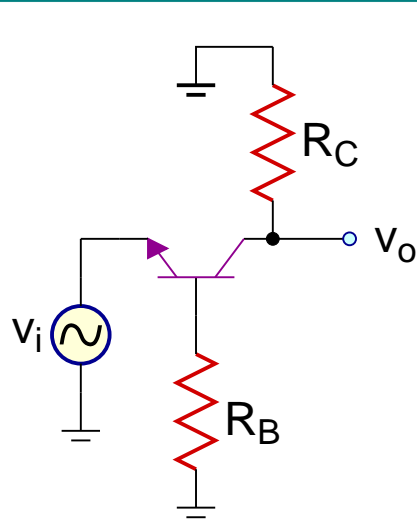
$$\frac{v_o}{v_i} = -\alpha \frac{R_C \parallel r_o}{r_e}$$



$$\frac{v_o}{v_i} = \frac{R_E \parallel r_o}{r_e + (R_E \parallel r_o)}$$

BJT Amplifiers

AC



$$G_m = g'_m + \frac{1}{r_o}$$

$$g'_m = g_m \frac{r_\pi}{r_\pi + R_B}$$

$$R_n = R_C \parallel r_o$$

$$\frac{v_o}{v_i} = G_m R_n$$

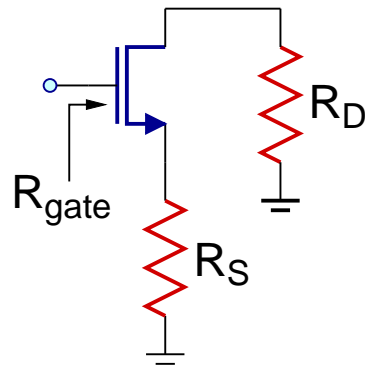
$$G_m = -g_m \frac{1 - \frac{R_E}{\beta r_o}}{1 + g_m R_E \left(1 + \frac{1}{\beta} + \frac{1}{g_m r_o} \right)}$$

$$\approx -\frac{g_m}{1 + g_m R_E}$$

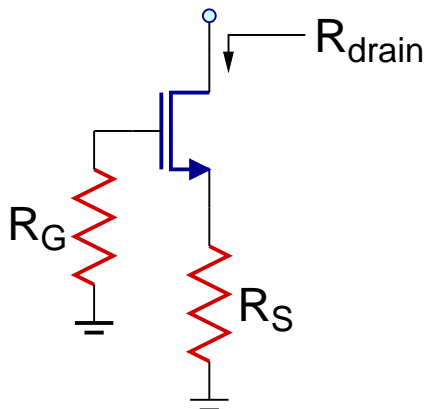
$$R_n = R_C \parallel [g_m r_o (R_E \parallel r_\pi) + r_o + (R_E \parallel r_\pi)]$$

$$\frac{v_o}{v_i} = G_m R_n$$

MOS Node Resistances

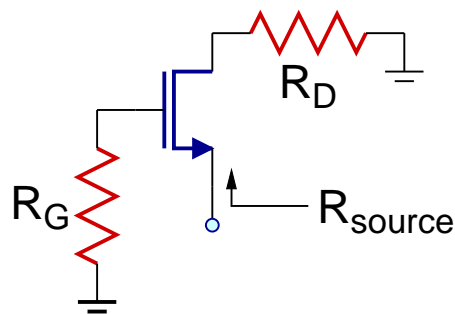


$$R_{\text{gate}} = \infty$$



$$R_{\text{drain}} = g'_m r_o R_S + r_o + R_S$$

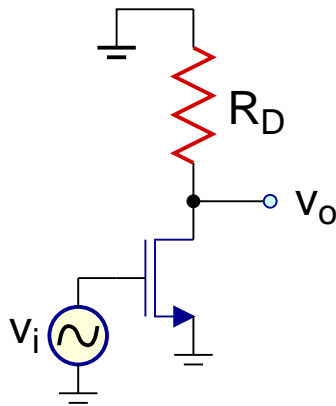
$$g'_m = g_m + g_{mb}$$



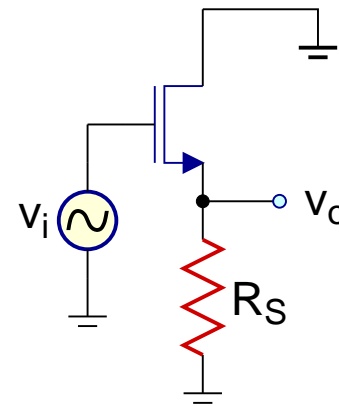
$$R_{\text{source}} = \left(\frac{1}{g'_m} \parallel r_o \right) \left(1 + \frac{R_D}{r_o} \right)$$

$$g'_m = g_m + g_{mb}$$

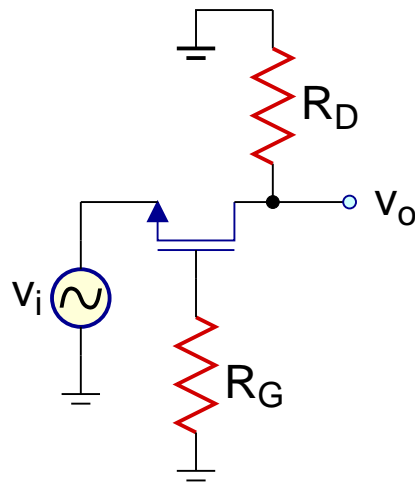
Calculation of $\mathbf{G_m}$ and $\mathbf{R_n}$ is not necessary if $\mathbf{r_o}$ is grounded, since it can be combined with either $\mathbf{R_D}$ or $\mathbf{R_S}$.



$$\frac{v_o}{v_i} = -\frac{R_D \parallel r_o}{\frac{1}{g_m}}$$



$$\frac{v_o}{v_i} = \frac{R_S \parallel r_o \parallel \frac{1}{g_{mb}}}{\frac{1}{g_m} + \left(R_S \parallel r_o \parallel \frac{1}{g_{mb}} \right)}$$

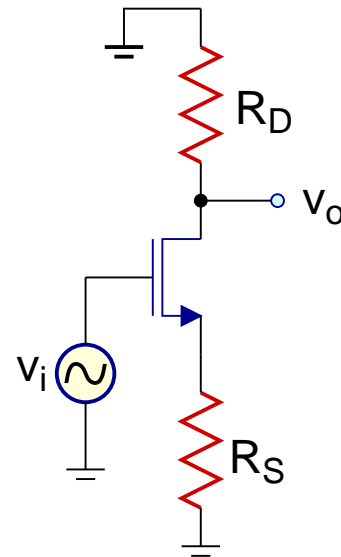


$$G_m = g'_m + \frac{1}{r_o}$$

$$g'_m = g_m + g_{mb}$$

$$R_n = R_D \parallel r_o$$

$$\frac{v_o}{v_i} = G_m R_n$$



$$G_m = -\frac{g_m}{1 + g'_m R_S + \frac{R_S}{r_o}}$$

$$g'_m = g_m + g_{mb}$$

$$R_n = R_D \parallel (g'_m r_o R_S + r_o + R_S)$$

$$\frac{v_o}{v_i} = G_m R_n$$