

# ECEN474/704: (Analog) VLSI Circuit Design Spring 2018

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## Lecture 12: Three Current Mirror OTA



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# Announcements

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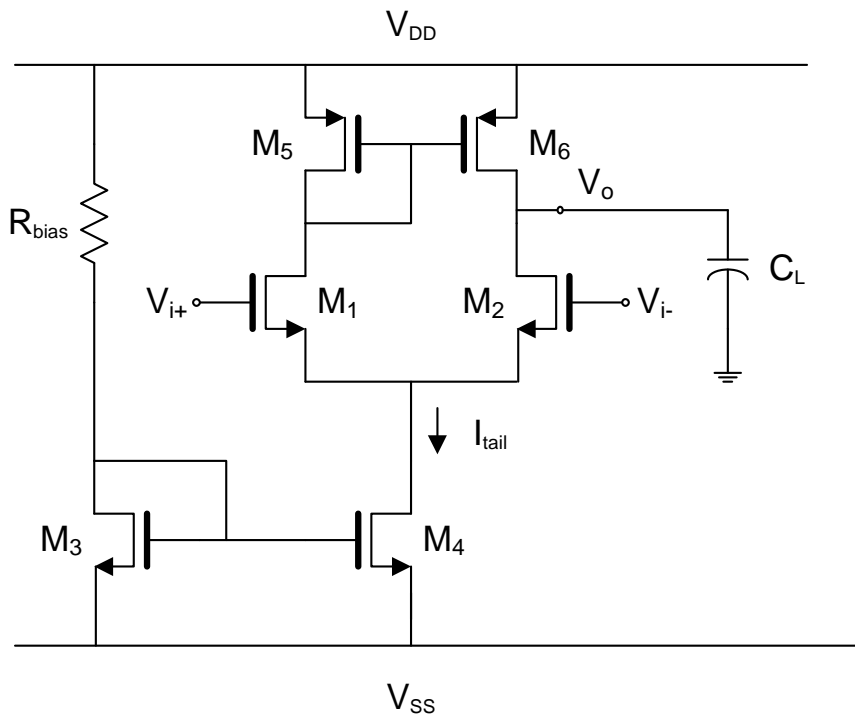
- HW3 is due today
- Exam dates reminder
  - Exam 2 is on Apr. 10
  - Exam 3 is on May 3 (3PM-5PM)

# Agenda

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- Simple OTA Review
- Three Current Mirror OTA Parameters
- Three Current Mirror OTA w/ Cascode Output

# Operational Transconductance Amplifier



$$\text{Transconductance } G_m = g_{m1} = \sqrt{KP_n \frac{W}{L_1} I_{TAIL}}$$

$$\text{Output Conductance } g_{out} = g_{o2} + g_{o6} = \frac{I_{TAIL}}{2} (\lambda_n + \lambda_p)$$

$$\text{DC Gain } A_v = G_m R_{out} = \frac{g_{m1}}{g_{o2} + g_{o6}} = \frac{2 \sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{\lambda_n + \lambda_p}$$

$$\text{Dominant Pole } \omega_{p1} = \frac{g_{o2} + g_{o6}}{C_L}$$

$$\text{Non-Dominant Pole } \omega_{p2} = \frac{g_{m6}}{C_M} \approx \frac{g_{mg}}{2C_{gs6}}$$

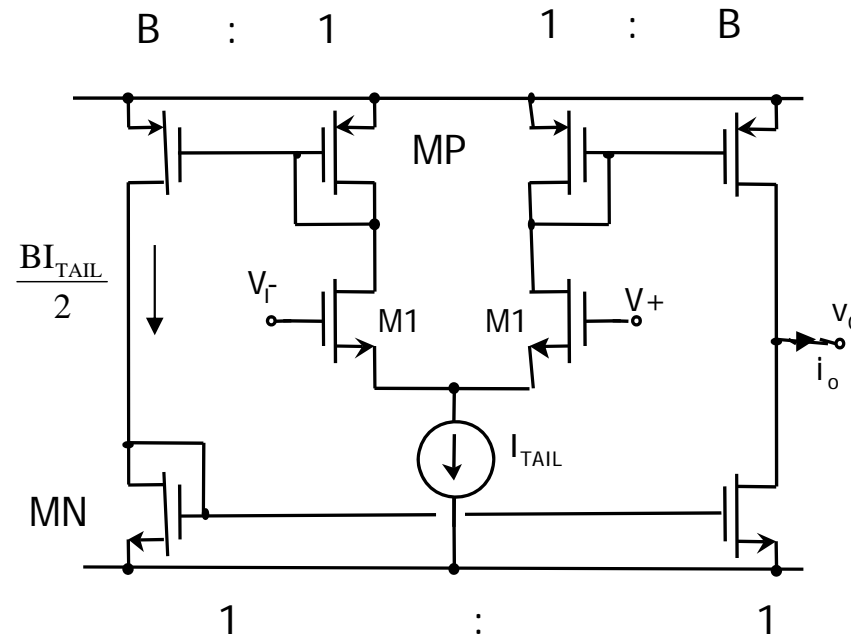
$$\text{Output Noise Current } i_{on}^2 = 2 \left( \frac{8}{3} kT \right) (g_{m1} + g_{m6})$$

$$\text{Input Noise Voltage } v_{in}^2 = 2 \left( \frac{8}{3} kT \right) \left( \frac{1}{g_{m1}} \right) \left( 1 + \frac{g_{m6}}{g_{m1}} \right)$$

$$GBW = \frac{G_m}{C_L} = \frac{\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{C_L}$$

$$\text{Slew Rate } SR = \frac{I_{tail}}{C_L}$$

# 3 Current Mirror OTA



- Relative to Simple OTA
  - Factor of "B" increase in  $G_m$ , GBW, and SR
  - Same  $A_v$
  - Slightly higher noise
  - Lower frequency non-dominant pole and third pole
  - $(B+1)$  times the power

### OTA based on 3 current mirrors

**Transconductance**  $G_m = Bg_{m1} = B\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}$

**Output Conductance**  $g_{out} = g_{on} + g_{op} = \frac{BI_{TAIL}}{2}(\lambda_n + \lambda_p)$

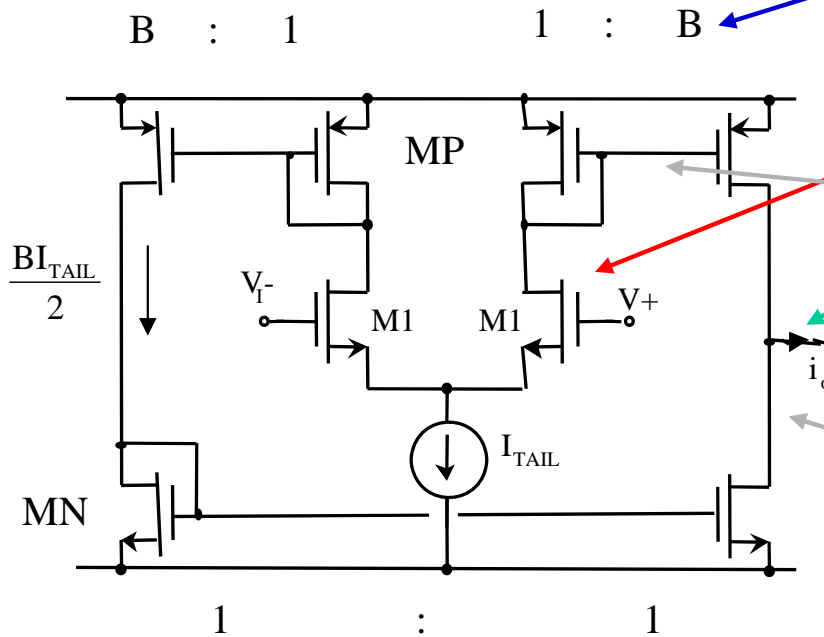
**DC Gain**  $A_v = G_m R_{out} = \frac{Bg_{m1}}{g_{on} + g_{op}} = \frac{2\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{\lambda_n + \lambda_p}$

**Dominant Pole**  $\omega_{p1} = \frac{g_{on} + g_{op}}{C_L}$

**Non-Dominant Pole**  $\omega_{p2} = \frac{g_{mp}}{C_{Mp}} \approx \frac{g_{mp}}{(1+B)C_{gsp}}$

**Gain - Bandwidth**  $GBW = \frac{G_m}{C_L} = \frac{B\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{C_L}$

**Slew Rate**  $SR = \frac{BI_{tail}}{C_L}$



## OTA based on 3 current mirrors

**Transconductance**  $G_m = Bg_{m1} = B\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}$

**Output Conductance**  $g_{out} = g_{on} + g_{op} = \frac{BI_{TAIL}}{2}(\lambda_n + \lambda_p)$

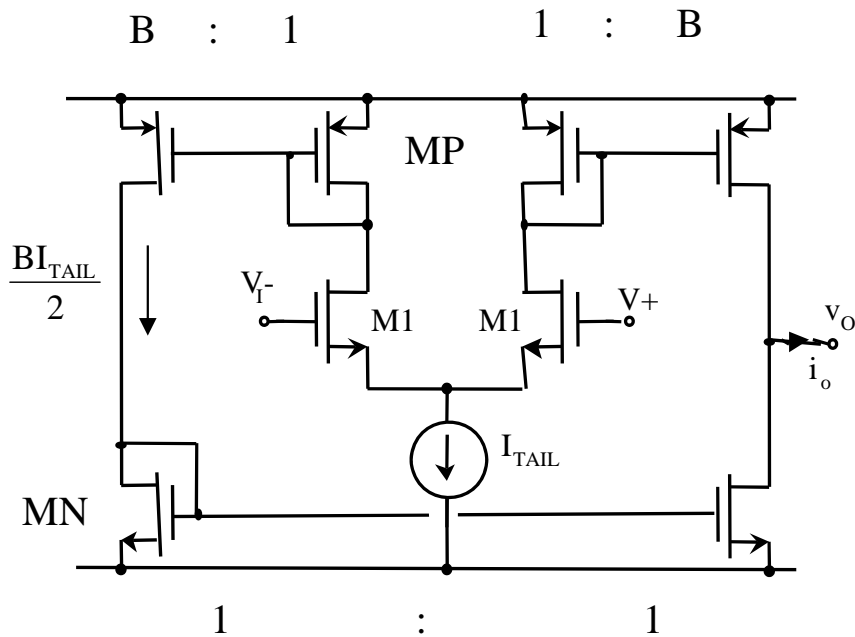
**DC Gain**  $A_v = G_m R_{out} = \frac{Bg_{m1}}{g_{on} + g_{op}} = \frac{2\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{\lambda_n + \lambda_p}$

**Dominant Pole**  $\omega_{p1} = \frac{g_{on} + g_{op}}{C_L}$

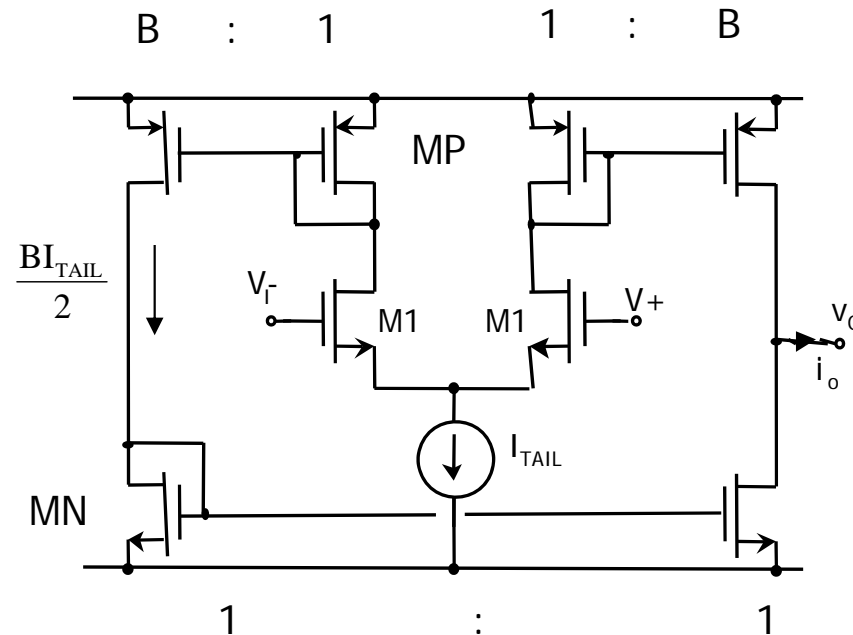
**Non - Dominant Pole**  $\omega_{p2} = \frac{g_{mp}}{C_{Mp}} \approx \frac{g_{mp}}{(1+B)C_{gsp}}$

**Gain - Bandwidth**  $GBW = \frac{G_m}{C_L} = \frac{B\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{C_L}$

**Slew Rate**  $SR = \frac{BI_{tail}}{C_L}$



# 3 Current Mirror OTA Noise

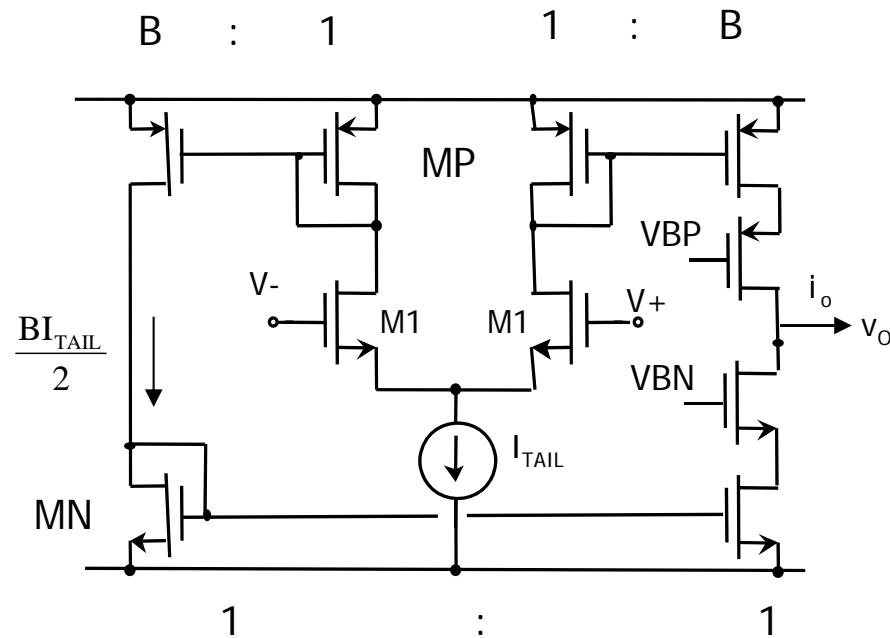


**Output Noise Current** 
$$i_{on}^2 = 2 \left( \frac{8}{3} kT \right) \left( B^2 g_{m1} + B^2 g_{mp} + B g_{mp} + g_{mn} \right)$$

**Input Noise Voltage** 
$$v_{in}^2 = 2 \left( \frac{8}{3} kT \right) \left( \frac{1}{g_{m1}} \right) \left( 1 + \frac{g_{mp}}{g_{m1}} \left( 1 + \frac{1}{B} \right) + \frac{g_{mn}}{B^2 g_{m1}} \right)$$

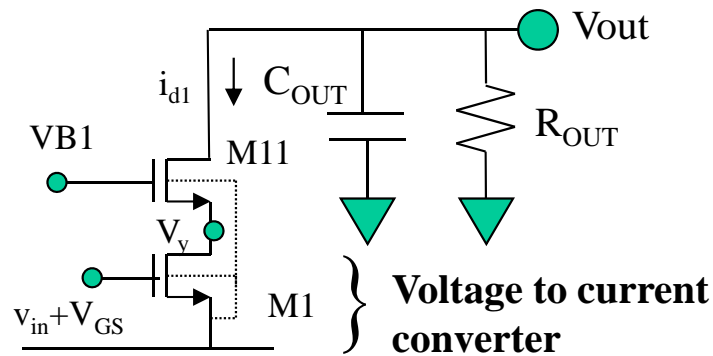


# 3 Current Mirror OTA w/ Cascode Output



- Relative to 3 Current Mirror OTA
  - Same  $G_m$ , GBW, and SR
  - $A_v$  increased by cascode  $g_{mc} r_{oc}$  factor
  - Approximately same noise
  - Introduce two additional cascode non-dominant poles
  - Same power

# Small Signal Analysis: Common-source Cascode Amplifier



AC analysis:

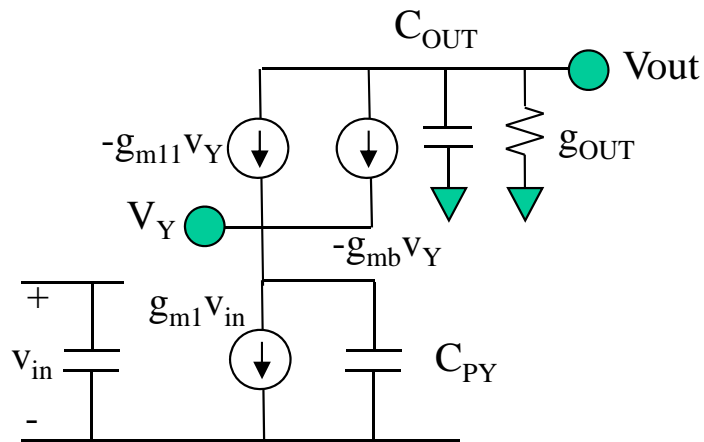
POLE AT  $V_Y$

$\Rightarrow$  Non-dominant pole:  $\cong$

$\Rightarrow \omega_{PND} = (g_{m11} + g_{mb11}) / C_{PY}$

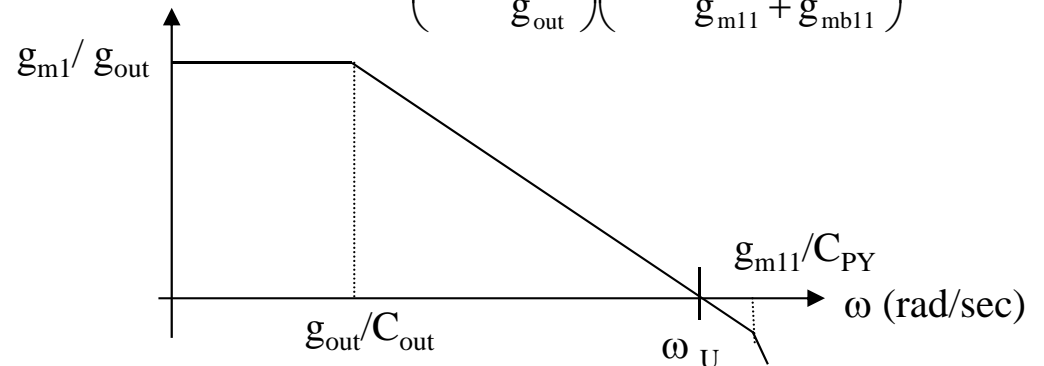
$\Rightarrow$  Dominant pole at  $1 / R_{OUT} C_{OUT}$

$\Rightarrow$  Transfer function

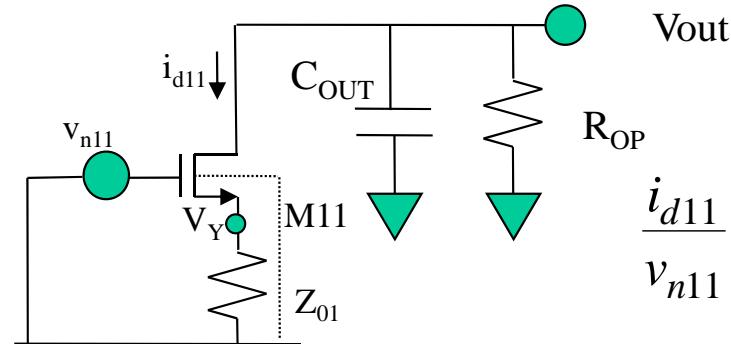
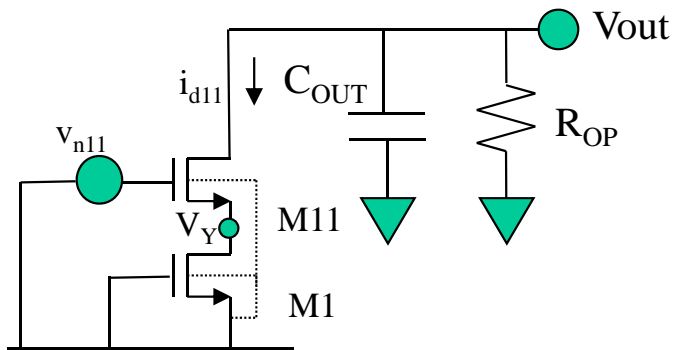


Small signal circuit

$$\frac{v_{out}}{v_{in}} = \left( -\frac{g_{m1}}{g_{out}} \right) \left( \frac{1}{1 + s \frac{C_{out}}{g_{out}}} \right) \left( \frac{1}{1 + s \frac{C_{PY}}{g_{m11} + g_{mb11}}} \right)$$



# Small Signal Analysis: Cascode Transistor



$$\frac{i_{d11}}{v_{n11}} = \left( \frac{g_{m11}}{1 + g_{m11}Z_{01}} \right)$$

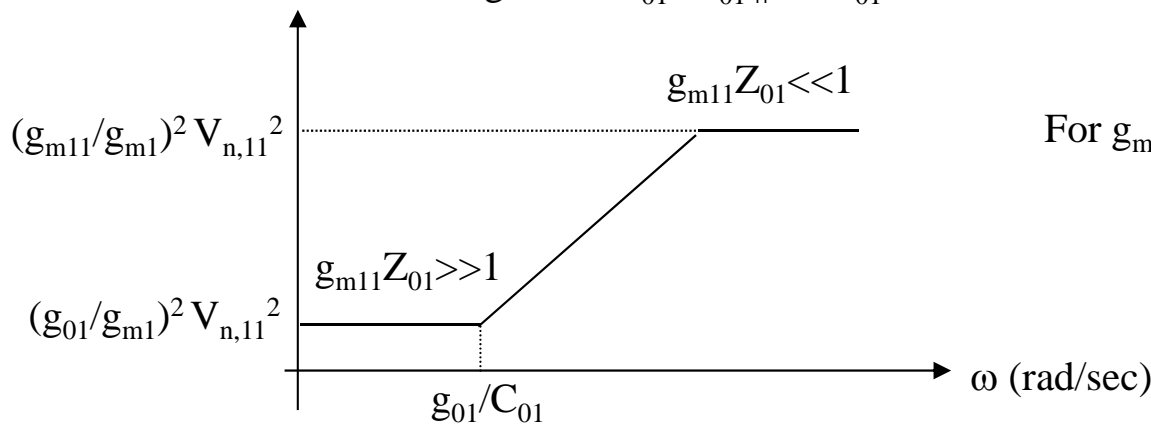
Input referred Noise:

$$v_{eqin,11}^2 = \frac{\left( \frac{g_{m11}}{1 + g_{m11}Z_{01}} \right)^2}{g_{m1}^2} v_{n,11}^2$$

For  $g_{m11}Z_{01} \gg 1$

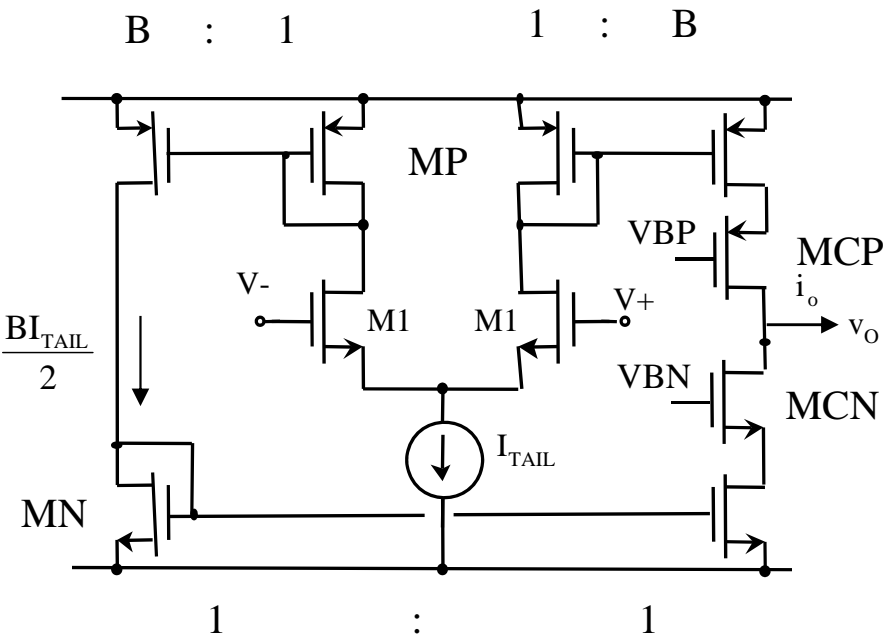
$$v_{eqin,11}^2 = \frac{1}{g_{m1}^2 Z_{01}^2} v_{n,11}^2$$

In general  $Z_{01} = R_{01} \parallel 1/sC_{01}$



- Cascode transistor noise can generally be neglected

## OTA based on 3 current mirrors using cascode transistors



**Current** =  $(1+B)I_{TAIL}$

**Transconductance**  $G_m = Bg_{m1} = B\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}$

**Output Conductance**  $g_{out} = \frac{g_{on}}{g_{mcn}r_{ocn}} + \frac{g_{op}}{g_{mcp}r_{ocp}} \approx \frac{BI_{TAIL}}{2g_{mc}r_{oc}} (\lambda_n + \lambda_p)$

**DC Gain**  $A_v = G_m R_{out} = \frac{Bg_{m1}g_{mc}r_{oc}}{g_{on} + g_{op}} = \frac{2\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{\lambda_n + \lambda_p} (g_{mc}r_{oc})$

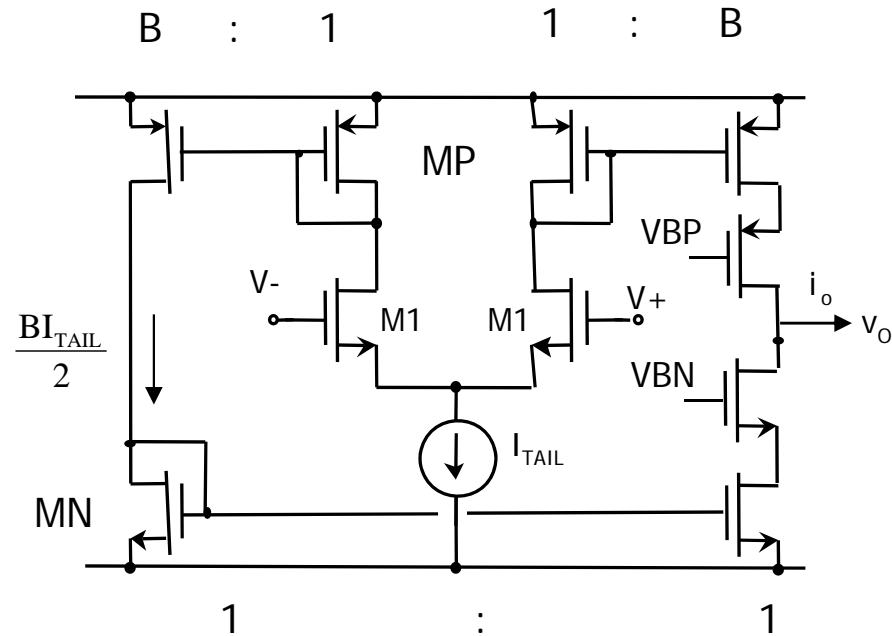
**Dominant Pole**  $\omega_{p1} = \frac{g_{on} + g_{op}}{g_{mc}r_{oc}C_L}$

**Non - Dominant Pole**  $\omega_{p2} = \frac{g_{mp}}{C_{Mp}} \approx \frac{g_{mp}}{(1+B)C_{gsp}}$

**Gain - Bandwidth**  $GBW = \frac{G_m}{C_L} = \frac{B\sqrt{KP_n \frac{W}{L_1} I_{TAIL}}}{C_L}$

**Slew Rate**  $SR = \frac{BI_{tail}}{C_L}$

# 3 Current Mirror OTA Noise

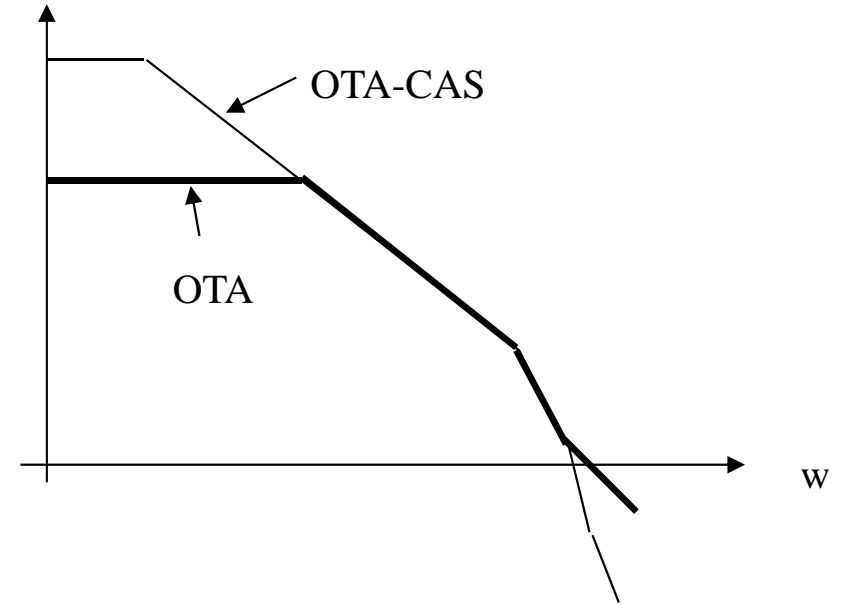
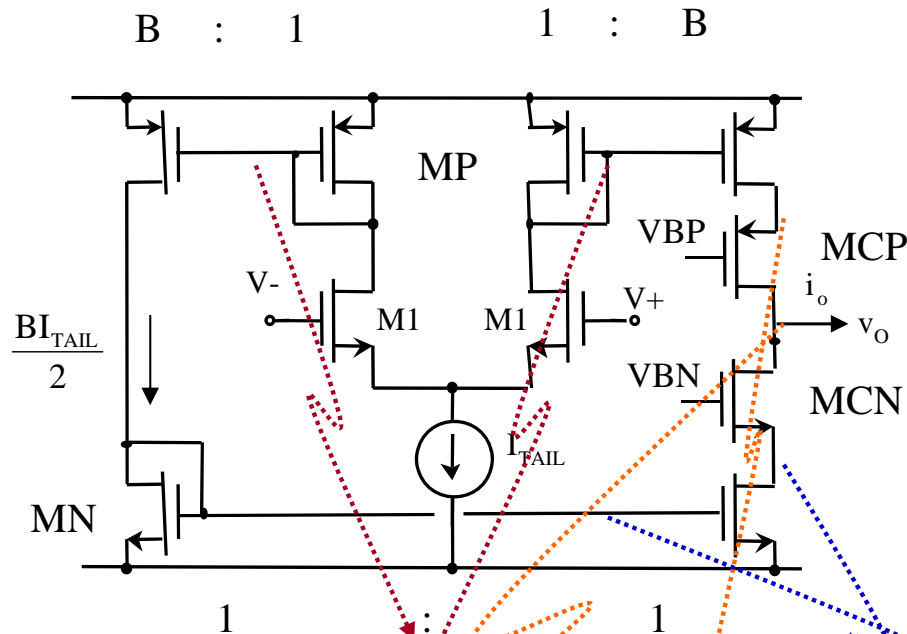


**Output Noise Current**  $i_{on}^2 = 2 \left( \frac{8}{3} kT \right) (B^2 g_{m1} + B^2 g_{mp} + B g_{mp} + g_{mn})$

**Input Noise Voltage**  $v_{in}^2 = 2 \left( \frac{8}{3} kT \right) \left( \frac{1}{g_{m1}} \right) \left( 1 + \frac{g_{mp}}{g_{m1}} \left( 1 + \frac{1}{B} \right) + \frac{g_{mn}}{B^2 g_{m1}} \right)$

- Cascode transistor contribution can be neglected
- Approximately equal to 3 current mirror OTA noise

## OTA based on 3 current mirrors using cascode transistors



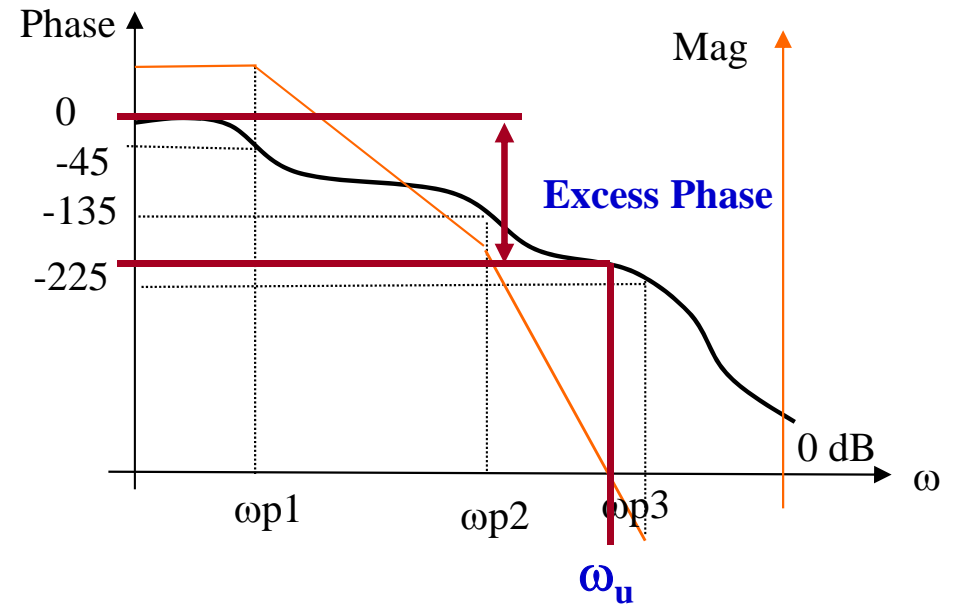
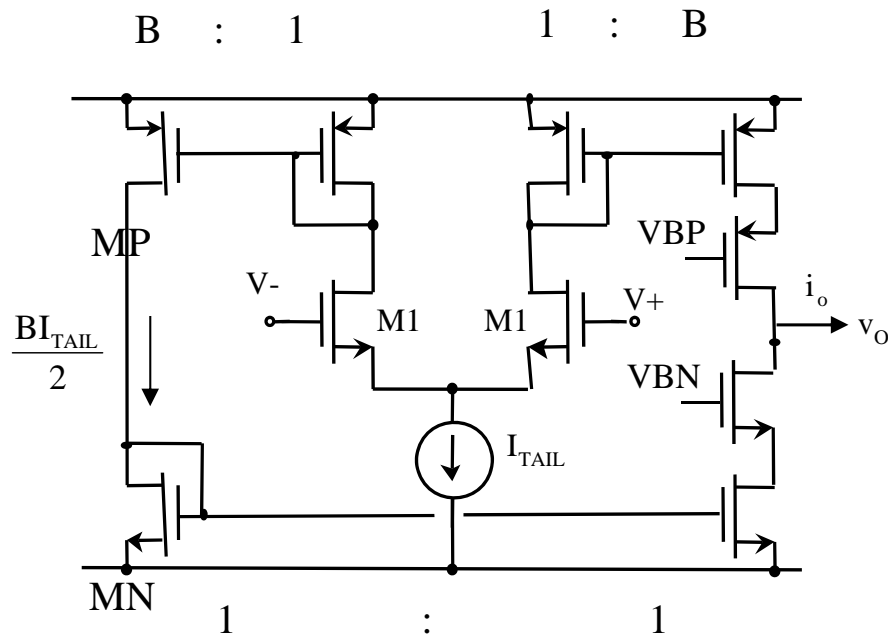
P-type current mirror    P-type cascode    N-type cascode    N-type current mirror

$$A_v \cong \frac{Bg_{m1}R_{out}}{1+sR_{out}C_{out}} \left[ \frac{1}{1+s\frac{(1+B)C_{GSP}}{g_{mP}}} \right] \left[ \frac{1}{1+s\frac{(1+\Delta)C_{GSCP}}{g_{mcp}}} + \left( \frac{1}{1+s\frac{(1+\Delta)C_{GSCN}}{g_{mcn}}} \right) \left( \frac{1}{1+s\frac{2C_{GSN}}{g_{mN}}} \right) \right]$$

**Phase Margin is limited**

OTA-output

## OTA based on 3 current mirrors using cascode transistors



**Excess Phase is defined as (phase at 0 - phase at  $\omega_u$ )**

**Phase Margin = (180 - excess phase)**

**Gain margin =  $\text{Gain}^{-1}$  measured at 180° excess phase**

# Next Time

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- Folded Cascode OTA
- Two Stage Miller OTA