# ECEN 605 LINEAR SYSTEMS

### Lecture 15

### State Feedback and Observers III – Observer Based Feedback

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# **Closed-lop Eigenvalues**

Suppose we calculate a state feedback u = Fx to place the eigenvalues of A + BF. Now we design an observer with eigenvalues of M chosen by us. From the observer we obtain  $\hat{x}$ . What if we close the loop with

$$u = F\hat{x}$$

instead of u = Fx? What are the closed loop eigenvalues? This answer is given by the so-called *Separation Principle*.

#### Theorem

The closed loop system under observed state feedback has eigenvalues

 $\lambda(A + BF) \cup \lambda(M).$ 

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(Proof of Separation Principle) Consider the general observer

 $\dot{z} = Mz + Ly + Gu.$ 

Let

$$z - Tx = e$$
.

Then

$$\dot{e} = Me + (MT - TA + LC)x + (G - TB)u.$$

Therefore to make z estimate Tx, we want  $e(t) \rightarrow 0$ . Thus, set

$$MT - TA + LC = 0 \tag{1}$$

$$G - TB = 0 \tag{2}$$

and

$$\lambda(M) \subset \mathbb{C}^-.$$

To estimate Fx we use the observer output

$$t := F\hat{x} = S_1z + S_2y$$
  
=  $(S_1T + S_2C)x + S_1\epsilon$ 

and set

$$S_1T + S_2C = F. ag{3}$$

The loop is closed by setting u = t (instead of u = Fx). Now look at the closed loop equations:

$$\dot{x} = Ax + Bu \dot{z} = Mz + Ly + Gu u = S_1z + S_2y.$$

We have

$$\begin{bmatrix} \dot{x} \\ \dot{z} \end{bmatrix} = \underbrace{\begin{bmatrix} A + BS_2C & BS_1 \\ LC + GS_2C & M + GS_1 \end{bmatrix}}_{A_{cl}} \begin{bmatrix} x \\ z \end{bmatrix}.$$
 (4)

Now make the coordinate transformation

$$\begin{bmatrix} x \\ z \end{bmatrix} = \begin{bmatrix} I & 0 \\ T & I \end{bmatrix} \begin{bmatrix} x \\ e \end{bmatrix}$$
$$\begin{bmatrix} x \\ e \end{bmatrix} = \begin{bmatrix} I & 0 \\ -T & I \end{bmatrix} \begin{bmatrix} x \\ z \end{bmatrix}.$$

Then using (1) - (4), we have

$$\begin{bmatrix} I & 0 \\ -T & I \end{bmatrix} A_{cI} \begin{bmatrix} I & 0 \\ T & I \end{bmatrix} = \begin{bmatrix} A + BF & BS_1 \\ 0 & M \end{bmatrix}$$

Therefore,

$$\lambda(A_{cl}) = \lambda(A + BF) \cup \lambda(M).$$

The transfer function of the observer as controller is derived as follows:

$$\dot{z} = Mz + Ly + Gu t = S_1 z + S_2 y \dot{z} = (M + GS_1)z + (L + GS_2)y$$

Therefore,

$$t(s) = \underbrace{\left[S_1(sI - M - GS_1)^{-1}(L + GS_2) + S_2\right]}_{C(s)} y(s)$$

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### Example

Consider the following single-input two-output system:

$$\dot{x} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix} x + \begin{bmatrix} 1 \\ 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} x$$

Design a full order observer with eigenvalues at -1, -2, -3 to estimate the state x.

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### Solution

$$A - LC = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{bmatrix} - \begin{bmatrix} l_{11} & l_{12} \\ l_{21} & l_{22} \\ l_{31} & l_{32} \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$
$$= \begin{bmatrix} -l_{11} & 1 & -l_{12} \\ -l_{21} & 0 & -l_{22} \\ 1 - l_{31} & 0 & -l_{32} \end{bmatrix}$$

One easy choice is:

$$l_{31} = 1$$
,  $l_{32} = 3$ ,  $s^2 + l_{11}s + l_{21} = s^2 + 3s + 2$ 

Thus, we have

$${\it l}_{11}=3,\ {\it l}_{21}=2,\ {\it l}_{12}, {\it l}_{22} {\rm ~arbitrary}, {\rm ~say}, \ 0.$$

 $L = \begin{bmatrix} 3 & 0 \\ 2 & 0 \\ 1 & 3 \end{bmatrix}$  $A - LC = \begin{bmatrix} -3 & 1 & 0 \\ -2 & 0 & 0 \\ 0 & 0 & -3 \end{bmatrix}$ 

Therefore, the observer is

Then

and

$$\dot{z} = \begin{bmatrix} -3 & 1 & 0 \\ -2 & 0 & 0 \\ 0 & 0 & -3 \end{bmatrix} z + \begin{bmatrix} 3 & 0 \\ 2 & 0 \\ 1 & 3 \end{bmatrix} y + \begin{bmatrix} 1 \\ 0 \\ 1 \end{bmatrix} u$$

 $z = \hat{x}$  is the estimate of x.

### Example

For the system given in the previous example, design a minimal order observer with eigenvalue at -3.

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Solution

$$y = \left[\begin{array}{c} y_1 \\ y_2 \end{array}\right] = \left[\begin{array}{c} x_1 \\ x_3 \end{array}\right] := \left[\begin{array}{c} \bar{x}_1 \\ \bar{x}_2 \end{array}\right]$$

Now

$$\begin{split} \dot{\bar{x}}_{1} &= \dot{x}_{1} = x_{2} + u = \bar{x}_{3} + u \\ \dot{\bar{x}}_{2} &= \dot{x}_{3} = x_{1} + u = \bar{x}_{1} + u \\ \dot{\bar{x}}_{3} &= \dot{x}_{2} = 0 \\ & \downarrow \\ \\ \begin{bmatrix} \dot{\bar{x}}_{1} \\ \dot{\bar{x}}_{2} \\ \dot{\bar{x}}_{3} \end{bmatrix} = \begin{bmatrix} 0 & 0 & \vdots & 1 \\ 1 & 0 & \vdots & 0 \\ \cdots & \cdots & \cdots \\ 0 & 0 & \vdots & 0 \end{bmatrix} \begin{bmatrix} \bar{x}_{1} \\ \bar{x}_{2} \\ \bar{x}_{3} \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \\ \cdots \\ 0 \end{bmatrix} u \\ \begin{bmatrix} y_{1} \\ y_{2} \end{bmatrix} = \begin{bmatrix} \bar{x}_{1} \\ \bar{x}_{2} \end{bmatrix} = \begin{bmatrix} 1 & 0 & \vdots & 0 \\ 0 & 1 & \vdots & 0 \\ 0 & 1 & \vdots & 0 \end{bmatrix} \begin{bmatrix} \bar{x}_{1} \\ \bar{x}_{2} \\ \bar{x}_{3} \end{bmatrix} + \underbrace{\begin{bmatrix} x_{1} \\ \bar{x}_{2} \\ \bar{x}_{3} \end{bmatrix}}_{(\bar{x})} = \underbrace{\begin{bmatrix} x_{1} \\ \bar{x}_{3} \end{bmatrix}}_{(\bar{x})} = \underbrace{\begin{bmatrix} x$$

Thus,

$$A_{11} = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} \qquad A_{12} = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \qquad B_1 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$$
$$A_{21} = \begin{bmatrix} 0 & 0 \end{bmatrix} \qquad A_{22} = 0 \qquad B_2 = 0$$

The observer is:

$$\dot{w}_2 = (A_{22} - L_2 A_{12})w_2 + [(A_{22} - L_2 A_{12})L_2 - L_2 A_{11} + A_{21}]y + (B_2 - L_2 B_1)u$$
  
$$\hat{x}_3 = w_2 - L_2 y.$$

Since the eigenvalue of  $A_{22} - L_2 A_{12}$  should be -3, we have

$$0 - \begin{bmatrix} l_{21} & l_{22} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} := -3$$

Here, we choose  $l_{21} = 3$  and  $l_{22} = 0$ . Therefore,

$$\dot{w}_2 = -3w_2 - 9y_1 - 3u \hat{x}_3 = w_2 + 3y_1 = \hat{x}_2.$$

Example

$$A = \left[ egin{array}{cc} 0 & 1 \ 0 & 0 \end{array} 
ight] \qquad b = \left[ egin{array}{cc} 0 \ 1 \end{array} 
ight] \qquad c = \left[ egin{array}{cc} 1 & 1 \end{array} 
ight]$$

i) Design a minimal order state estimator with its pole at -1.

$$\dot{x} = Ax + bu$$
  $y = cx$ 

We need to pick T so that

$$cV = \begin{bmatrix} 1 & 0 \end{bmatrix}$$

We choose

$$V = \begin{bmatrix} 1 & 1 \\ 0 & -1 \end{bmatrix} \quad \text{and} \quad V^{-1} = \begin{bmatrix} 1 & 1 \\ 0 & -1 \end{bmatrix}$$

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So, we have new coordinate system with V as follows:

$$\dot{\bar{x}} = \bar{A}\bar{x} + \bar{b}u$$
  $y = \bar{c}\bar{x}$ 

where

$$\bar{A} = V^{-1}AV = \begin{bmatrix} 0 & \vdots & -1 \\ \cdots & \cdots \\ 0 & \vdots & 0 \end{bmatrix} \qquad \bar{b} = V^{-1}B = \begin{bmatrix} 1 \\ \cdots \\ -1 \end{bmatrix}$$
$$\bar{c} = cV = \begin{bmatrix} 1 & \vdots & 0 \end{bmatrix}.$$

The minimal order state estimator equation is

$$\dot{w} = (\bar{A}_{22} - L_2 \bar{A}_{12})w + \left[(\bar{A}_{22} - L_2 \bar{A}_{12})L_2 + L_2 \bar{A}_{11} + \bar{A}_{21}\right]y + (\bar{b}_2 - L_2 \bar{b}_1)u$$

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Let us select  $L_2$  such that

$$\lambda(\bar{A}_{22}-L_2\bar{A}_{12})=-1.$$

Then we have  $L_2 = -1$ . Therefore, the minimal order state estimator becomes

$$\dot{w} = -w + y$$
$$\hat{x}_2 = w + L_2 y.$$

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ii) Combine the state feedback and the observer into an output feedback controllor, and give the state equations as well as the transfer function of this controller. Choose a state feedback to assign poles of the original system at all -1.

Now we need to consider the coordinate transformation.

$$\hat{x} = V\hat{x}, \quad y = \bar{c}\bar{x}, \quad w = \hat{x}_2 - L_2 y$$

$$\begin{bmatrix} y \\ w \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ -L_2 & 1 \end{bmatrix} \underbrace{\begin{bmatrix} \bar{x}_1 \\ \hat{x}_2 \end{bmatrix}}_{\hat{x}}.$$

Thus,

$$\hat{x} = V\hat{x} = V \begin{bmatrix} 1 & 0 \\ L_2 & 1 \end{bmatrix} \begin{bmatrix} y \\ w \end{bmatrix}$$
$$= \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} y \\ w \end{bmatrix}$$

From the control law,  $f = \begin{bmatrix} f_1 & f_2 \end{bmatrix} = \begin{bmatrix} -1 & -2 \end{bmatrix}$  which assigns the original poles at -1, we have

$$u = F\hat{x} = \begin{bmatrix} -1 & -2 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} y \\ w \end{bmatrix}$$
$$= -3y + 2w.$$

Therefore, the controller state equations are:

$$\dot{w} = -w + y$$
$$u = F\hat{x} = 2w - 3y$$

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and the controller transfer function is:

$$G(s) = c(sI - A)^{-1}b + d$$
  
= 2(s + 1)^{-1}1 + (-3)  
=  $\frac{2}{s+1} - 3$   
=  $\frac{-3s - 1}{s+1}$ .

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Example

Consider a system

$$A = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \qquad B = \begin{bmatrix} 1 & 0 \\ 0 & -1 \\ 1 & 1 \end{bmatrix} \qquad C = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}.$$

Let a full order observer be

$$\dot{z} = Mz + Ly + Gu$$
  
 $\hat{x} = Pz + Qy.$ 

We choose the observer poles

$$\Lambda_o = \{-0.1, -0.2, -0.3\}\,,$$

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then from M = A - LC, we have

$$L = \left[ \begin{array}{rrr} 1.1998 & -0.0008 \\ -0.0148 & 0.0301 \\ -0.0644 & 0.4002 \end{array} \right]$$

and

$$M = A - LC = \begin{bmatrix} -0.1998 & 0 & 0.0008\\ 0.0148 & 0 & -0.0301\\ 0.0644 & 1 & -0.4002 \end{bmatrix}$$

Thus, the observer equations are (seting G = B, P = I, Q = R = 0)

$$\dot{z} = \begin{bmatrix} -0.1998 & 0 & 0.0008\\ 0.0148 & 0 & -0.0301\\ 0.0644 & 1 & -0.4002 \end{bmatrix} z + \begin{bmatrix} 1.1998 & -0.0008\\ -0.0148 & 0.0301\\ -0.0644 & 0.4002 \end{bmatrix} y + \begin{bmatrix} 1 & 0\\ 0 & -1\\ 1 & 1 \end{bmatrix} u$$

$$\hat{x} = \begin{bmatrix} 1 & 0 & 0\\ 0 & 1 & 0\\ 0 & 0 & 1 \end{bmatrix} z.$$

$$(5)$$

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The first figure in Figure 1 shows the plots of the states x(t) and the estimated states  $\hat{x}(t)$ . This shows all three states are estimated correctly. To close look at the convergence, we plot the error state

$$e(t) = \hat{x}(t) - x(t)$$

in the second figure of Figure 1 which shows the convergence. The initial conditions of these plot were:

$$x(0) = [0 - 1 - 2]$$
 and  $z(0) = [-5 \ 0 \ 5]$ .

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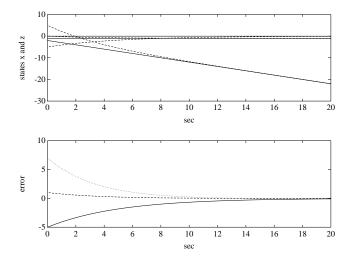


Figure 1: x(t),  $\hat{x}(t)$ , and e(t) (x(0) = [0 - 1 - 2])

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Now let us choose a different initial conditions: we choose

$$x(0) = [1 \ 2 \ 3]$$

while maintaining z(0) the same. The state x(t) and  $\hat{x}(t)$  are shown in Figure 2. The error e(t) is also shown.

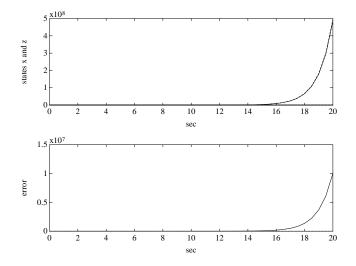


Figure 2: x(t),  $\hat{x}(t)$ , and e(t) (Problem 3:  $x(0) = [1 \ 2 \ 3]$ )

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This shows that the estimated states do not converge to the true states. Obviously the full order observer we designed does not function properly. This interesting fact can be explained in terms of the robustness of the observer.